

# Neutronics Codes Currently Used in Japan for Fast and Thermal Reactor Applications

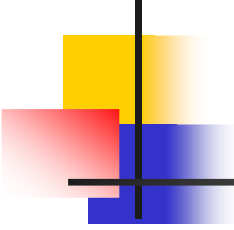
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## Contents

1. Introduction
2. BWRs in Japan
3. PWRs in Japan
4. FR Analysis Codes
5. General Analysis Codes
6. Future Plan and Conclusions



# 1. Introduction

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- BWR

  - Operating 29

  - Under construction 3

- PWR

  - Operation 23

  - Under construction 1

- FR

  - Monju

  - JOYO

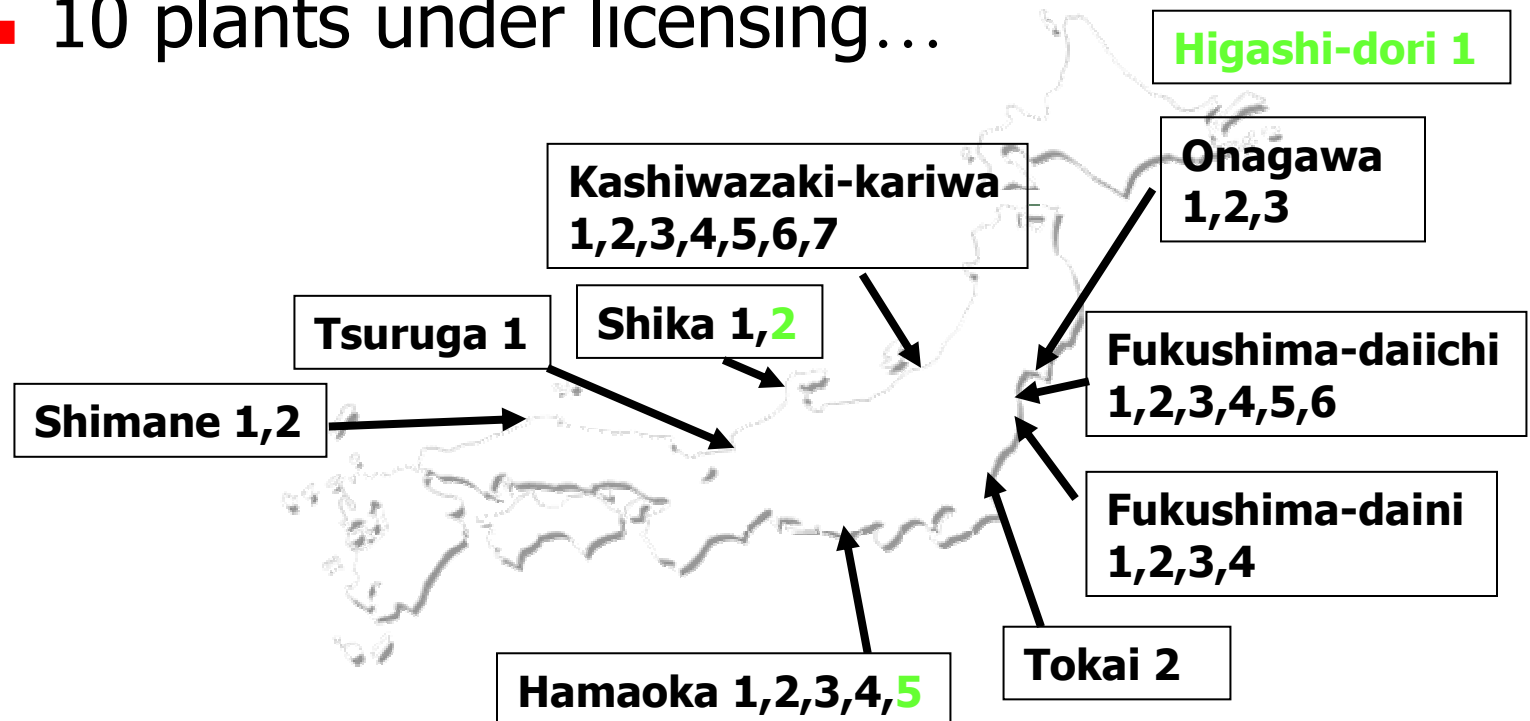
- Experimental Reactor

  - JEARI

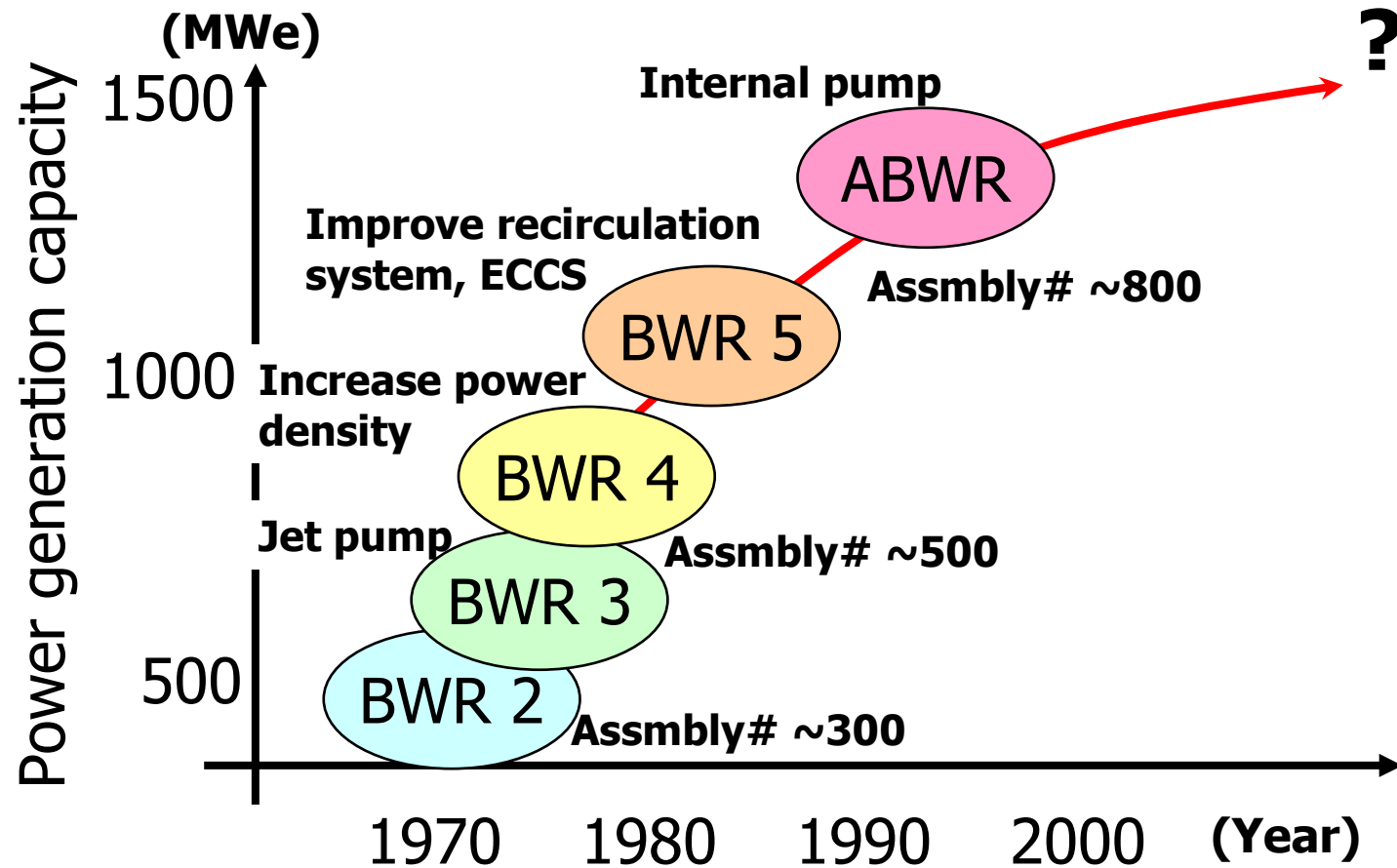
  - University

## 2. BWRs in Japan

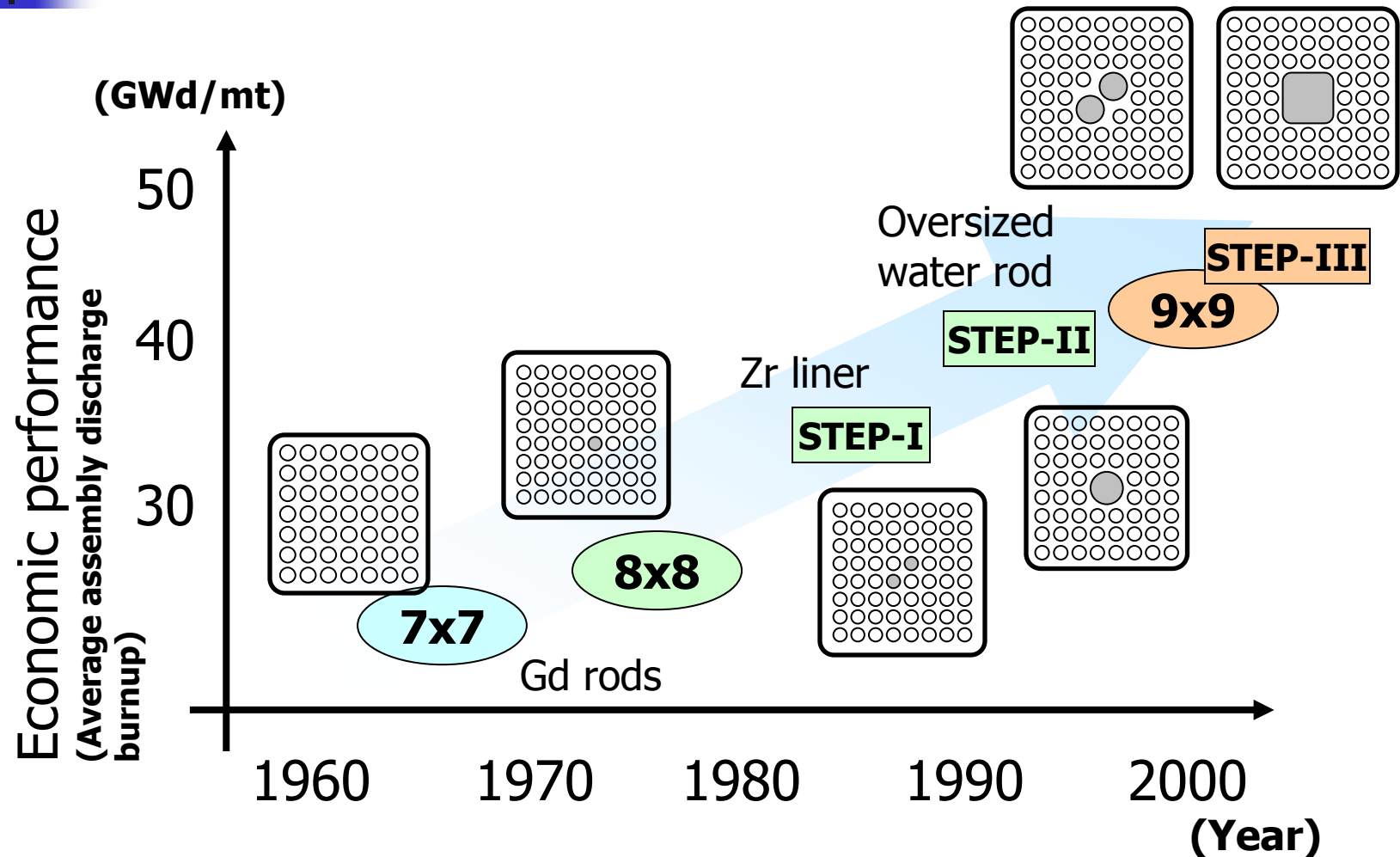
- Status of Japanese BWRs
  - 29 plants operating (BWR-2,3,4,5,ABWR)
  - 3 plants under construction (BWR-5,ABWR)
  - 10 plants under licensing...

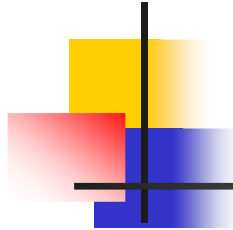


# History of Japanese BWRs



# History of BWR Fuels





# Core simulators

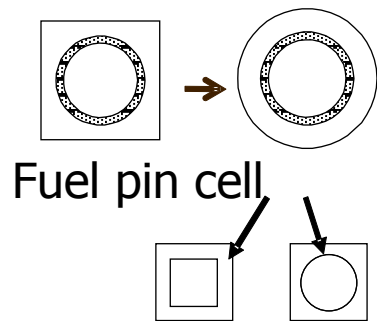
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- BWR core simulators and users

|                                        |
|----------------------------------------|
| <b>Code share in<br/>reload design</b> |
|----------------------------------------|

- |                              |      |
|------------------------------|------|
| ■ TGBLA/LOGOS, TGBLA/PANACEA | ~48% |
| ■ GNF-J, GIS                 |      |
| ■ CASMO/SIMULATE             | ~45% |
| ■ TEPSYS, TOiNX              |      |
| ■ NEUPHYS/COS3D              | ~7%  |
| ■ NFI, CTI                   |      |

# BWR core calculation

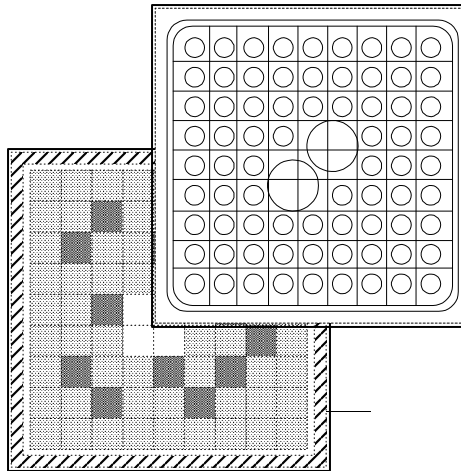
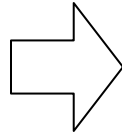


Fuel pin cell

**Effective macroscopic cross sections**

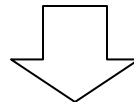
## Pin cell calculation

- Cylindrical transport calculation
- Fine energy groups
- Resonance calculation

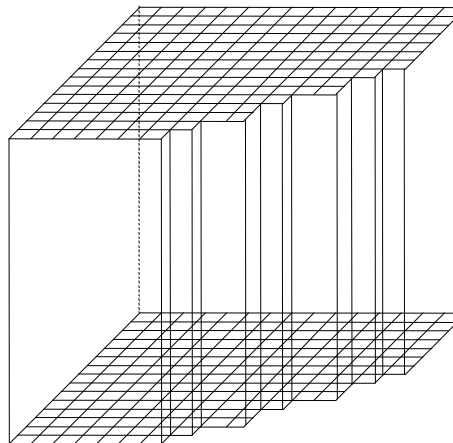


## Assembly calculation

- 2D calculation
- Few/several energy groups
- Diffusion/transport theory
- Homo/heterogeneous geometry

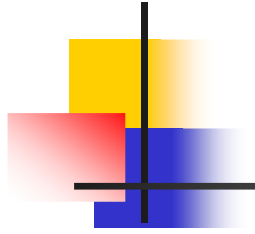


**Assembly constants**



## Core calculation

- 3D calculation
- few energy groups
- diffusion theory
- FDM/ANEM
- Void feedback
- Doppler feedback



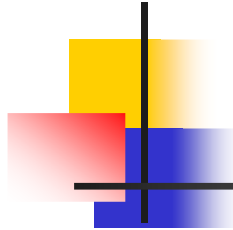
# TEPSYS

## CASMO/SIMULATE system

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- Developed by Studsvik Scandpower (SSP)
- Vendor-independent code system
- Standard core simulator of TEPSYS
  - BWR reload core design
  - Fuel bid evaluation
  - On-line core monitoring system (adaptive model)

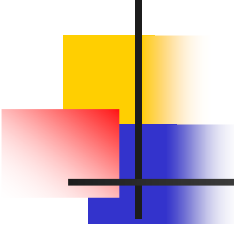
**A subsidiary of Tokyo  
Electric Power Company**



# Experiences

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- Applied more than 70 reload cycles to 13 TEPCO BWR plants from 1988
- Introduced CASMO/SIMULATE core monitoring system to 2 TEPCO BWR plants in 1999 and 2002



# Computational methods used in CASMO/SIMULATE

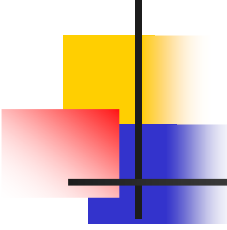
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## ■ CASMO

- Pin cell transport + Assembly transport
- Explicit geometry analysis by Method of Characteristics (MOC)
- Extended version (Capability of 2D whole core analysis) (2000~)

## ■ SIMULATE

- Advanced nodal expansion method (ANEM)
- BWR enhancement models (2000~)



# Enhancement models for BWR analysis

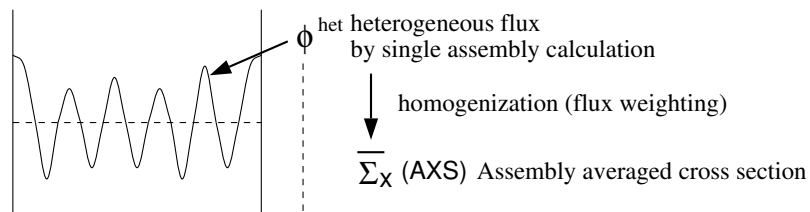
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- Spatial rehomogenization model
  - Correction of assembly averaged cross section (spatially)
- Fast leakage model
  - Correction of collapsed cross section (energy spectrally)
- Dynamic discontinuity factor model
  - ADF adjustment by empirical procedure
  - Determined by results of reference explicit geometry transport core calculations

# Spatial rehomogenization

## Single assembly calculation

fundamental mode



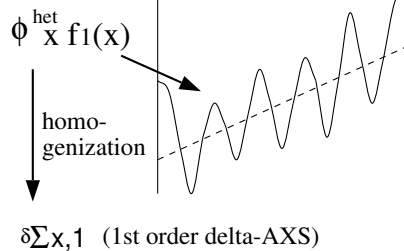
nodal expansion function

$$\begin{aligned} f_1(x) &= x \\ f_2(x) &= 3x^2 - 1/4 \\ f_3(x) &= x^3 - x/4 \\ f_4(x) &= x^4 - 3/10 x^2 - 1/80 \end{aligned}$$

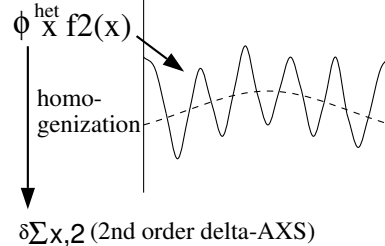
higher-order cross sections

$$\delta\Sigma_{X,n} \quad (n=1,4)$$

1st order



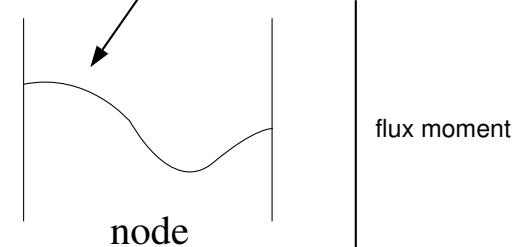
2nd order



## Nodal core calculation

intra nodal flux

$$\phi^{hom}(x) = \phi_0 + \phi_1 f_1(x) + \phi_2 f_2(x) + \phi_3 f_3(x) + \phi_4 f_4(x)$$



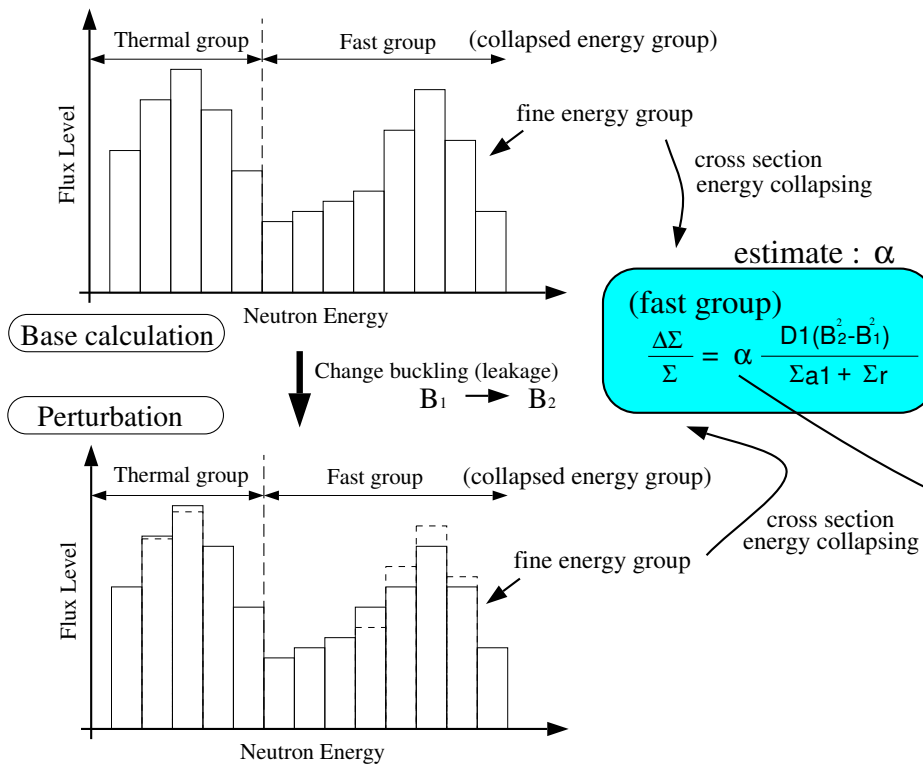
re-homogenization

$$\Sigma_X^* = \bar{\Sigma}_X + \sum_{(n=1,4)} \phi_n \delta\Sigma_{X,n}$$

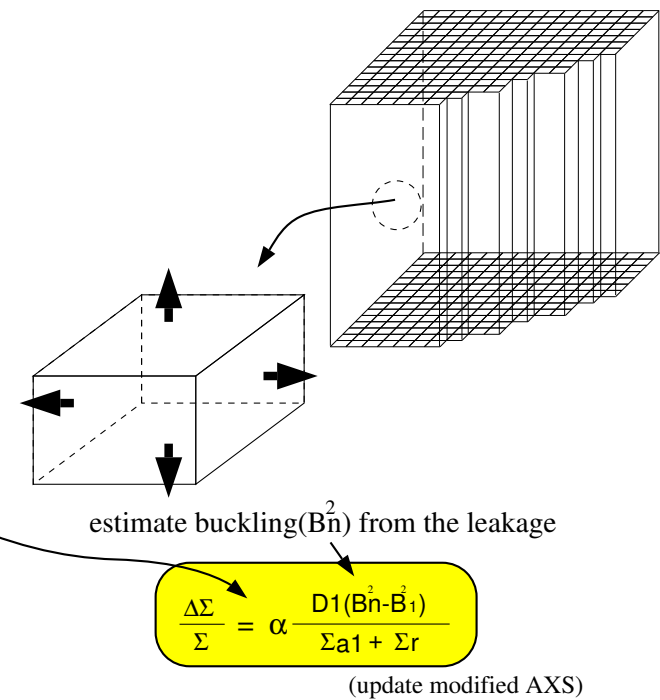
(update modified AXS)

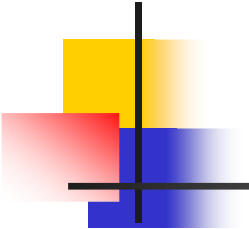
# Fast leakage model

## Single assembly calculation



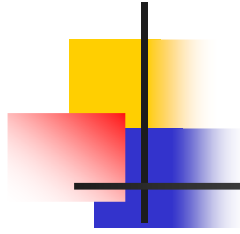
## Nodal core calculation





## Verification of SIMULATE neutronics model vs CASMO-4 reference core analyses

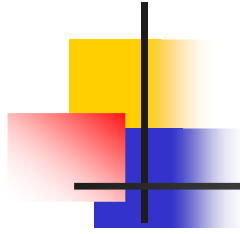
| Case          | RMS of Assembly Powers(%) |          | Error in rod worth (pcm) |          |
|---------------|---------------------------|----------|--------------------------|----------|
|               | Standard                  | Enhanced | Standard                 | Enhanced |
| BOC Un-Rodded | 1.36                      | 0.76     | -22                      | +10      |
| BOC Rodded    | 1.52                      | 0.59     |                          |          |
| MOC Un-Rodded | 1.33                      | 0.59     | +49                      | +0       |
| MOC Rodded    | 1.70                      | 0.53     |                          |          |
| EOC Un-Rodded | 1.33                      | 0.59     | -26                      | -8       |
| EOC Rodded    | 1.57                      | 0.64     |                          |          |



# Global Nuclear Fuel Japan

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- A joint Venture of GE, Toshiba & Hitachi
  - In, January 2000, GNF-J started as a part of Global Nuclear Fuel LLC – A joint venture of GE, Toshiba & Hitachi.
  - GE Nuclear Fuel Joined as GNF-A
  - GNF provides nuclear fuel and services, from fuel design, manufacturing to the core management



# Lattice Physics Code in GNF-J

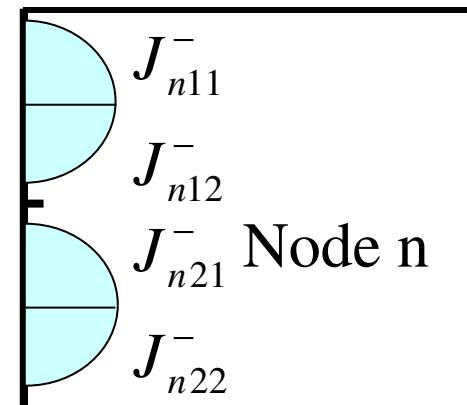
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- TGBLA(1979-2004)
  - Pin transport + assembly diffusion
  - L-method (1984) accounts for spectrum mismatch effects in pin transport calc.
  - Gd rod asymmetric depletion (1987)
  - RICM option solves ultra-fine group slowing down for resonance shielding (1987)

# Lattice Physics Code in GNF-J

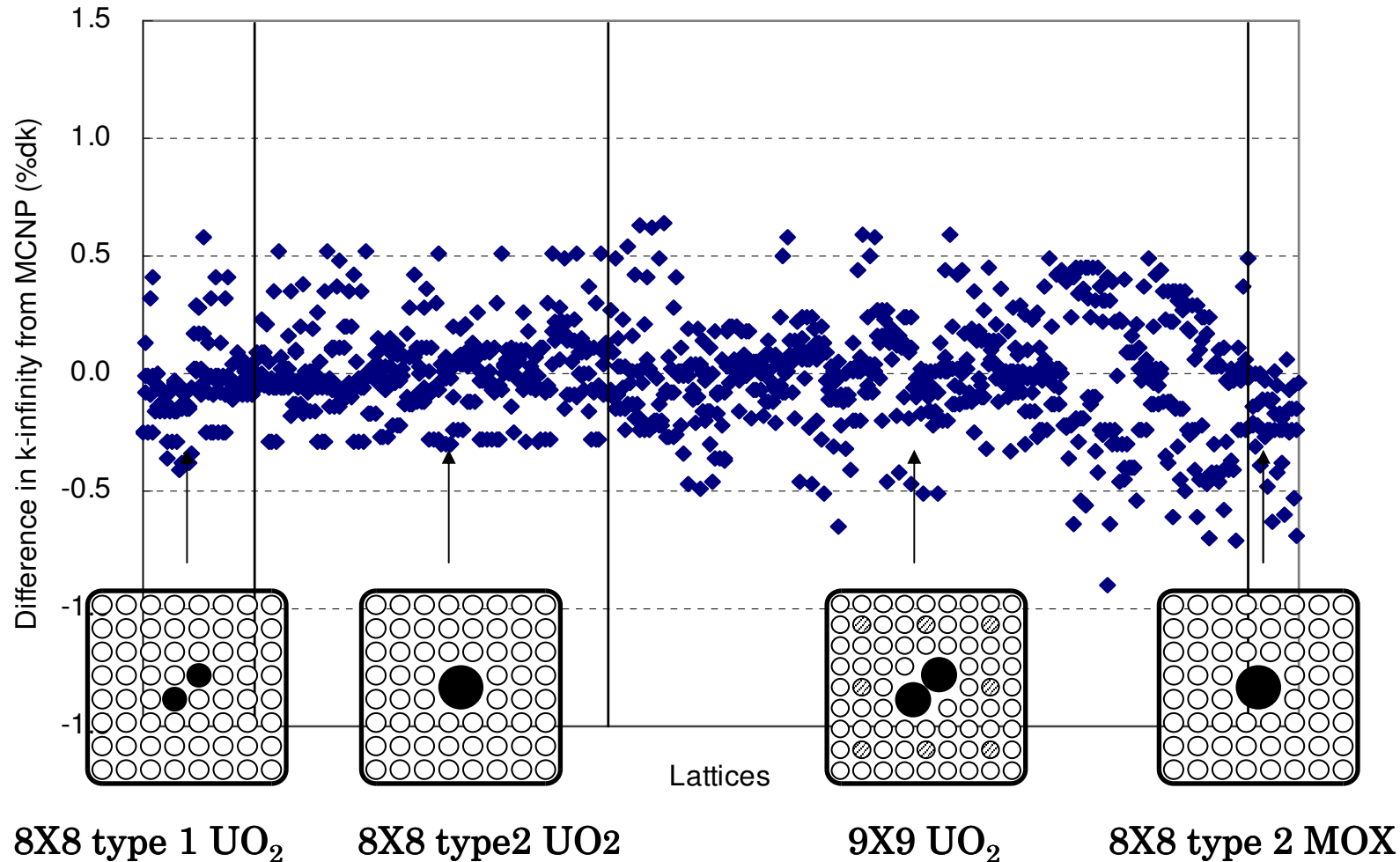
- LANCER(2000-)

- Improved CCCP method yields sufficient accuracy within reasonable computing costs.
- 35 energy group 2D flux calculation provides accurate solution for highly heterogeneous lattices
- Interface currents are expanded with 2 spatial X 2 angular modes.



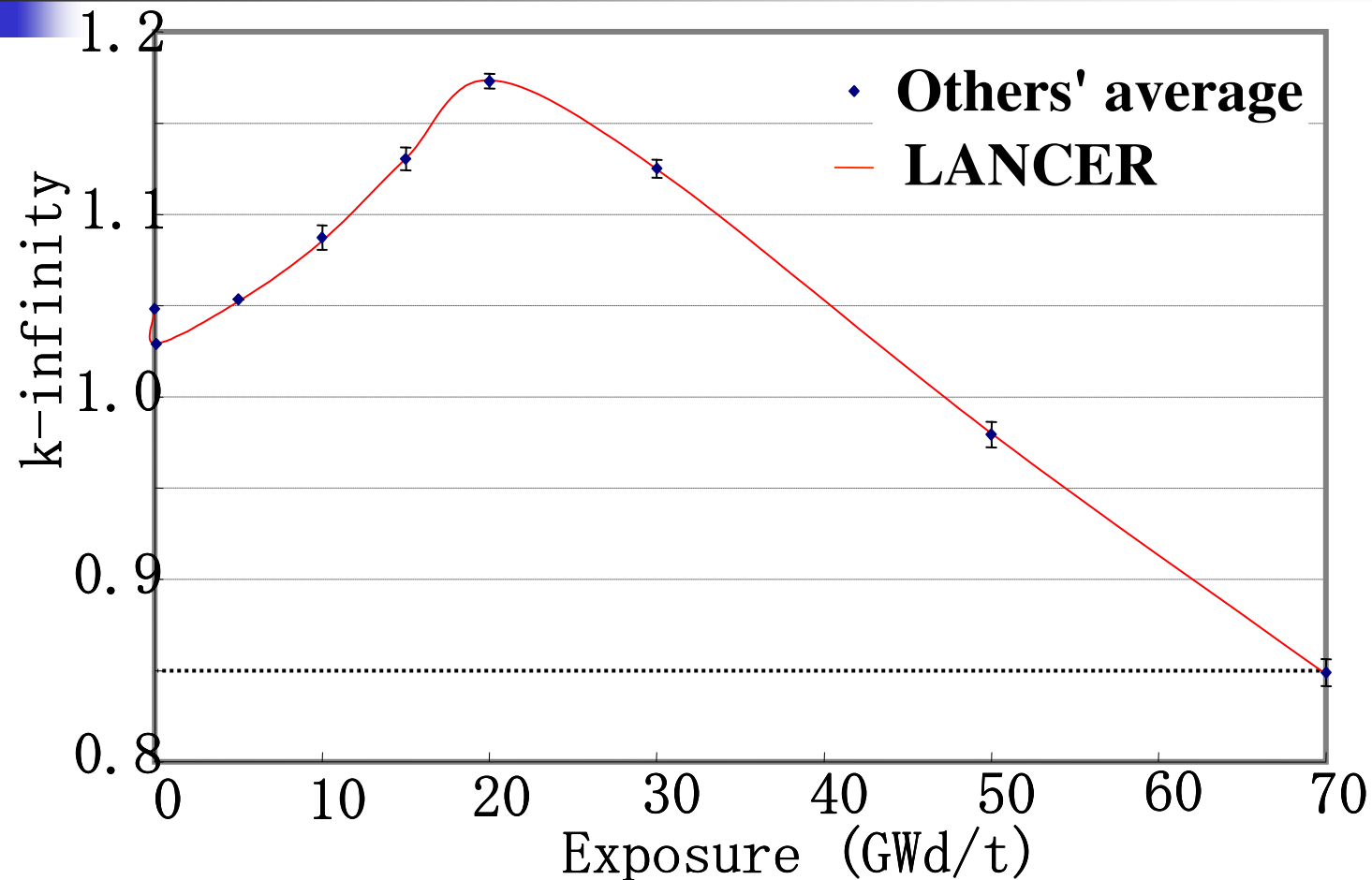


# Lattice Physics Code in GNF-J

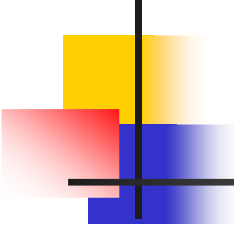


**Error in K-inf to MCNP4C in BOL Fuel Lattices**

# Lattice Physics Code in GNF-J



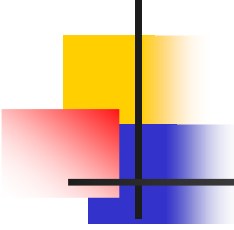
**K-inf of AESJ Benchmark UO2 Assembly**



# Core Physics Code in GNF-J

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- LOGOS(1992-2004)
  - Developed based on PANACEA (GE).
  - Improved 1.5 group (quasi 2-group) model solves intranodal thermal flux analytically, accounts for spectral mismatch effects between assemblies
  - Pin power reconstruction model based on the analytic thermal flux expansion.
- PANACEA v.11 (1997-2004)
  - Almost the same improvements as LOGOS

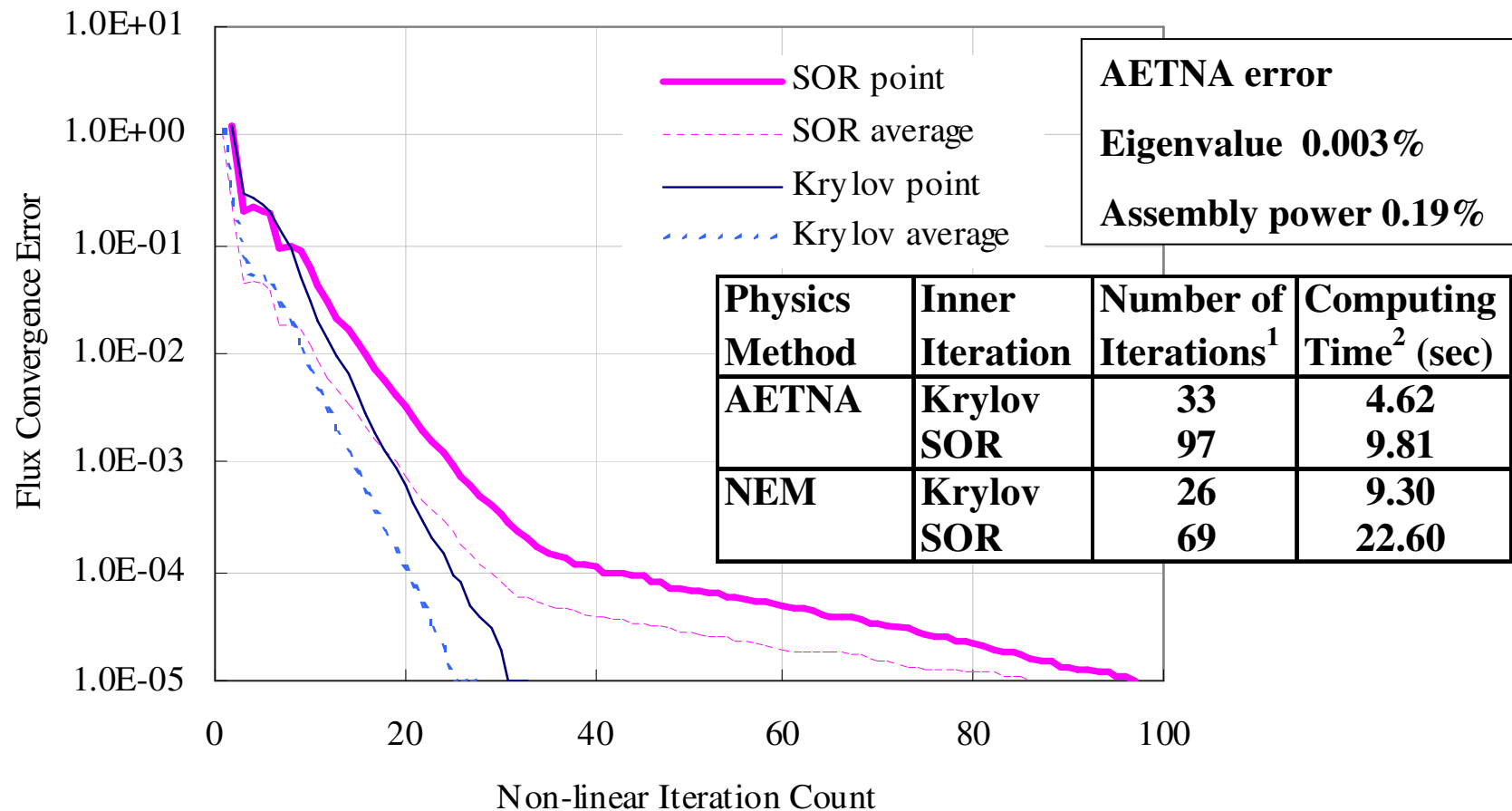


# Core Physics Code in GNF-J

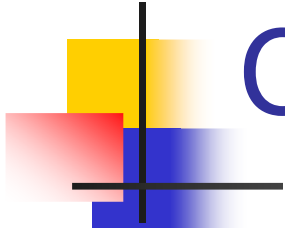
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- AETNA (2000-)
  - 3 group analytic-polynomial nodal expansion method with iterative expansion coefficient update.
  - Krylov (GMRES) method for inner iteration along with NODEX type non-linear eigenvalue iteration provides faster convergence
  - Consistent pin power reconstruction model to the flux solution.
  - Pu-241 tracking model for decay correction

# Core Physics Code in GNF-J

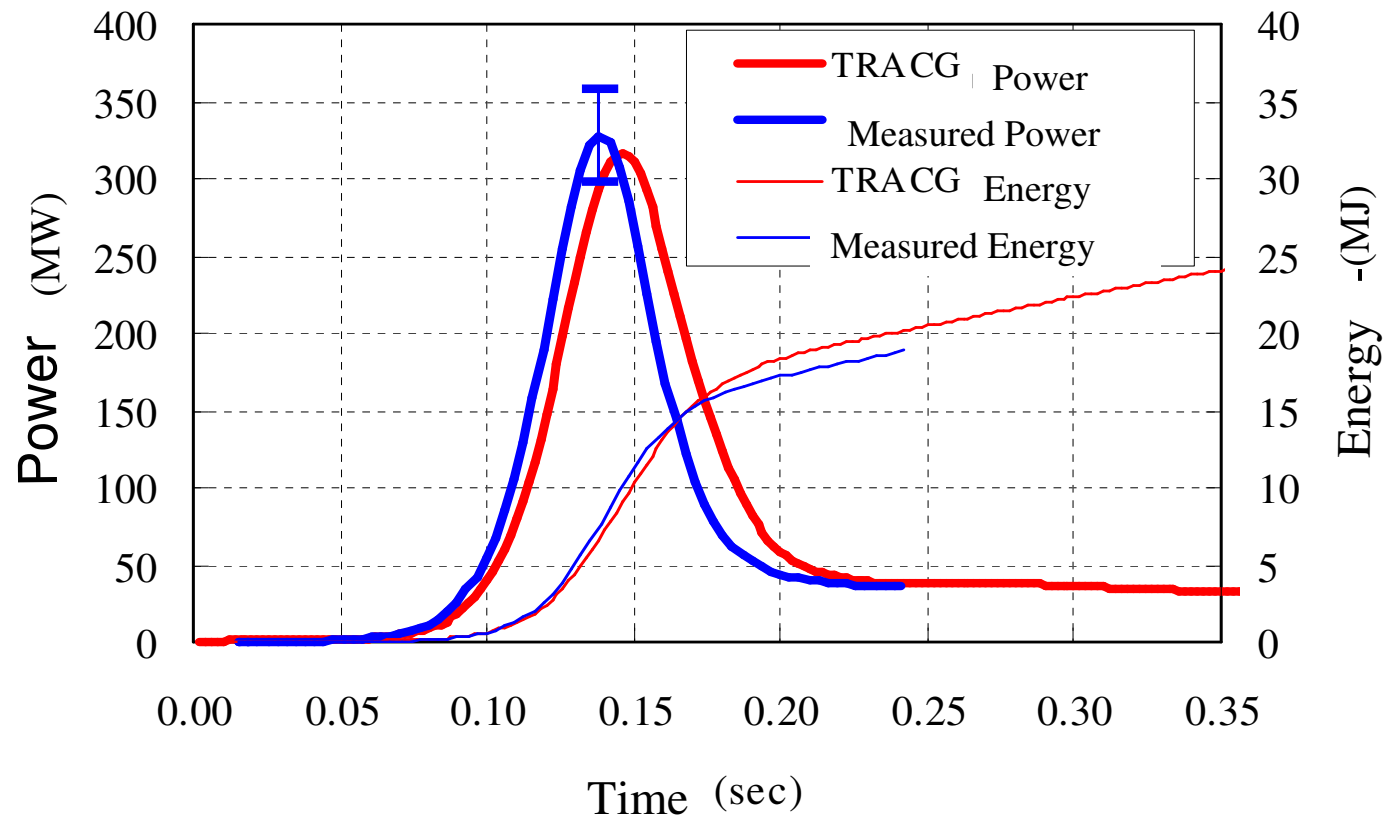


***LRA 3D BWR Static Benchmark***

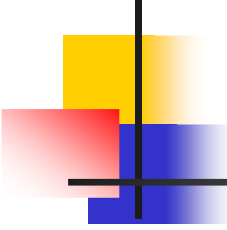


# Core Physics Code in GNF-J

***AETNA/TRACG05 coupled nuclear thermal hydraulics code for plant transient analysis***



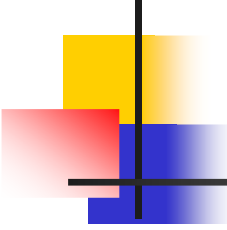
***SPERT III E-core RIA Test-81 (hot standby)***



# BWR Analysis Codes; NFI

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- Nuclear Fuel Industries, Ltd.'s Standard Neutronics Code System
  - Assembly Analysis Code : **NEUPHYS**
    - Fine Group Collision Probability Calculation +
    - Three Groups Diffusion Model
  - BWR Core Simulator : **COS3D**
    - Modified One Group Diffusion Model
    - Power Correction with Spectrum Mismatch Model



# BWR Analysis Codes; NFI

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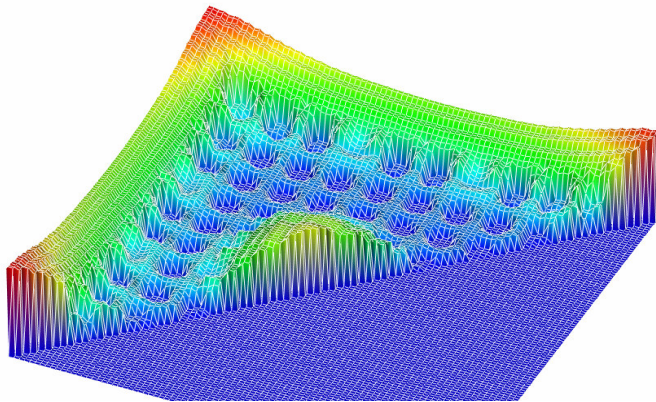
- Applications of NFI Standard System
  - Design of 9X9 type B Assembly
    - Average Discharge Burnup 45GWD/t
    - Assembly Maximum Burnup 55GWD/t
  - BWR Core Management system
- For Further Advanced, More Complex and More Heterogeneous Design
  - NFI Supplies Advanced Neutronics Code System

# BWR Analysis Codes; NFI

## ■ Advanced NFI Neutronics Codes

### ■ Assembly Analysis Code

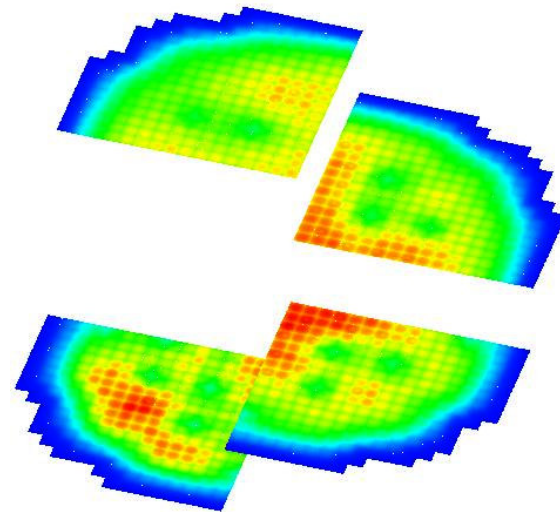
- Arbitrary Geometry Multigroup MOC
- Brand New Cross Section Library Based on JENDL-3.2



Thermal Flux Distribution

### ■ BWR Core Simulator

- Few Groups Advanced Nodal Method Core Calculation
- Intra-Nodal Exposure and Spectrum History Distribution Model

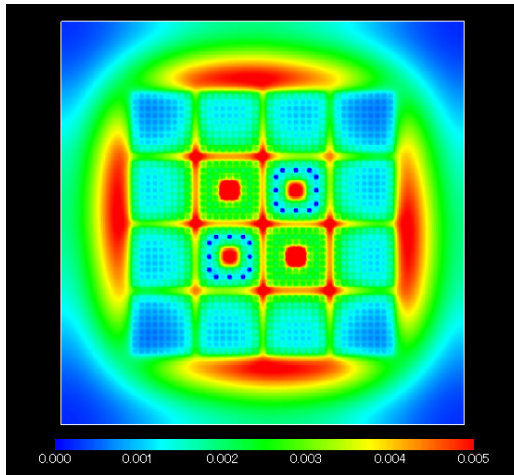


Axial Depending Whole Core Fast Flux Distribution

# BWR Analysis Codes; NFI

## Critical Experimental Analysis

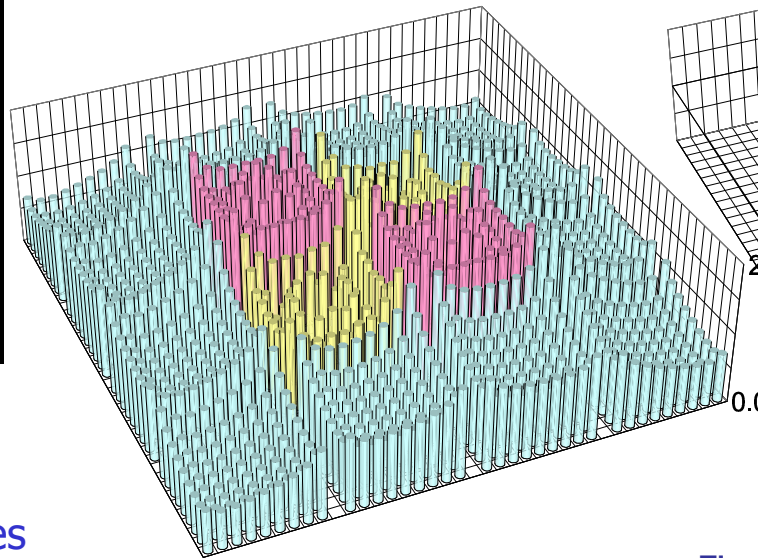
(Comparison with Monte-Carlo Calculation in 2-D Geometry)



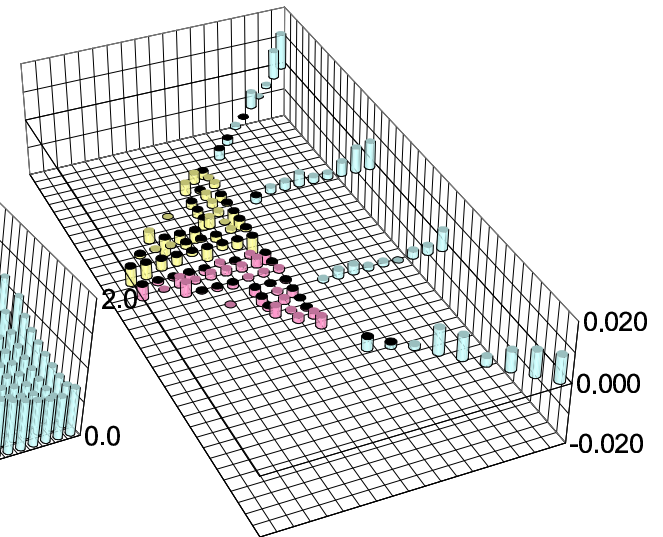
Thermal flux distribution

### CONFIGURATION

- Three Types of Assemblies
  - 9X9 UO<sub>2</sub> Driver
  - 9X9 with Large Water Channel
  - 9X9 W/C and Twelve Gd rod
- Water Reflector



Fission Rate Distribution



Fission Rate Relative Differences  
(NFI System-GMVP)

R.M.S=0.0035

### 3. PWRs in JAPAN

#### Operating : 23

2-Loop plant : 8

3-Loop plant : 8

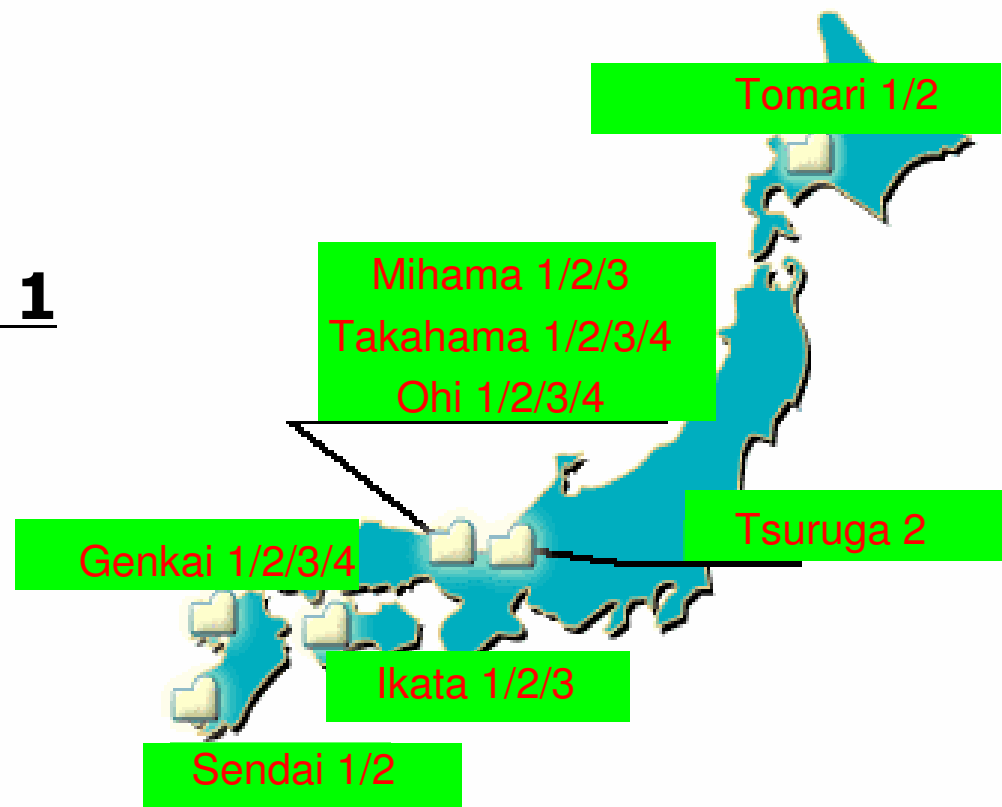
4-Loop plant : 7

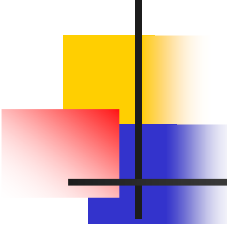
#### Under Construction : 1

Tomari 3 (3-Loop)

#### Under Licensing : 2

Tsuruga 3&4 (APWR)

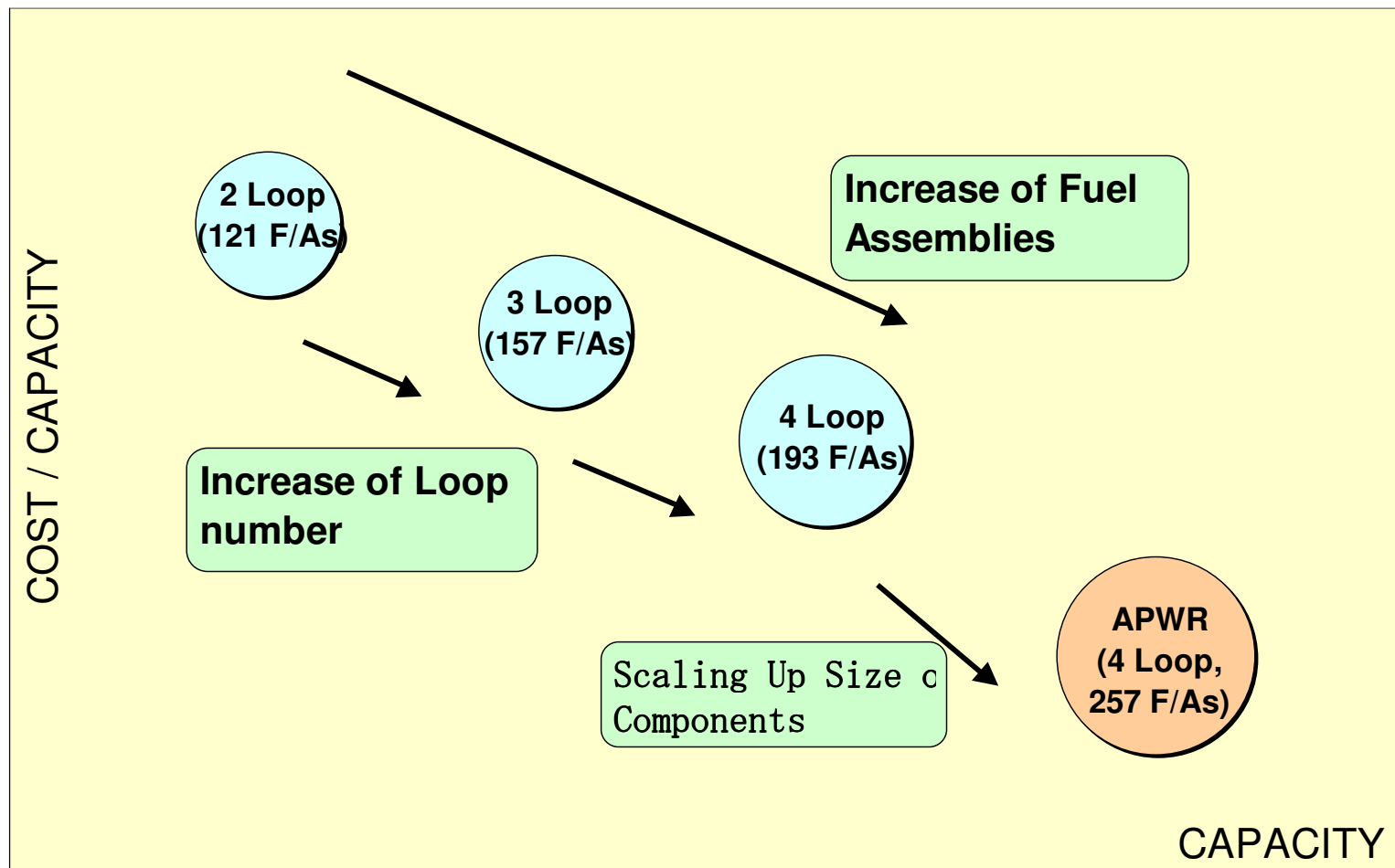




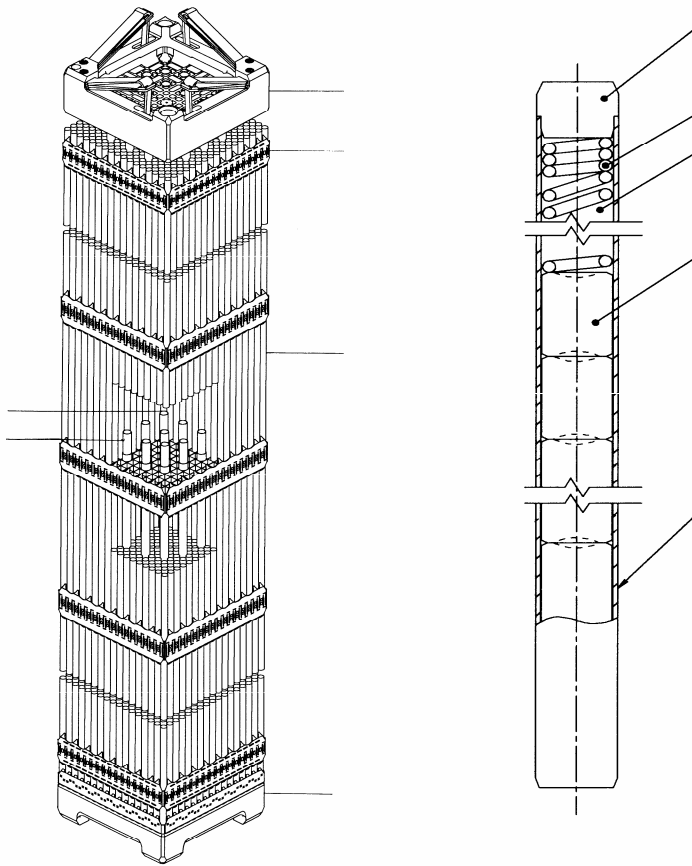
# Main Specifications (1/3)

| Parameters                      | Conventional PWR |       |       |       | APWR  |
|---------------------------------|------------------|-------|-------|-------|-------|
| No. of primary coolant loop     | 2                | 3     | 3     | 4     | 4     |
| Thermal output(MWt)             | 1,650            | 2,432 | 2,652 | 3,411 | 4,451 |
| No. of fuel assemblies          | 121              | 157   | 157   | 193   | 257   |
| Core equivalent diameters(m)    | 2.46             | 3.04  | 3.04  | 3.37  | 3.89  |
| Fuel length(m)                  | 3.66             | 3.66  | 3.66  | 3.66  | 3.66  |
| Fuel type                       | 14x14            | 15x15 | 17x17 | 17x17 | 17x17 |
| Ave. linear power density(kW/m) | 20.4             | 20.3  | 17.1  | 17.9  | 17.6  |
| Fuel rod diameter(mm)           | 10.7             | 10.7  | 9.5   | 9.5   | 9.5   |
| No. of control rods             | 29               | 48    | 48    | 53    | 69    |

# Main Specifications (2/3)

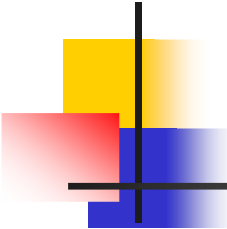


# Main Specifications (3/3)



|                                  | 14x14 | 15x15 | 17x17             |
|----------------------------------|-------|-------|-------------------|
| Fuel rod diameter (mm)           | 10.7  | 10.7  | 9.5               |
| Pellet diameter (mm)             | 9.3   | 9.3   | 8.2               |
| Fuel length (m)                  | 3.66  | 3.66  | 3.66              |
| Ave. linear power density (kW/m) | 20.4  | 20.3  | 17.1<br>~<br>17.9 |

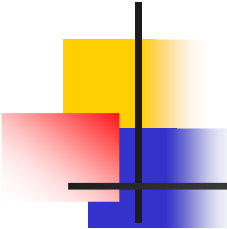
**Overview of fuel assembly and fuel rod (17x17-type)**



# Improvement in economical efficiency in conventional PWRs (1/2)

## BURNUP LIMIT and CYCLE LENGTH

|                               | ~1990           | 1990~2004        | 2004~             |
|-------------------------------|-----------------|------------------|-------------------|
| Burnup Limit of Fuel Assembly | 39 GWd/t        | 48 GWd/t         | 55 GWd/t          |
| Fuel Enrichment               | 3.2~3.4         | 4.1              | 4.8               |
| Cycle Length                  | 9~12 months     | 12~13 months     | 13 ~ months       |
| Type of Burnable Absorber     | Cluster-type BP | Mainly Gd (6wt%) | Mainly Gd (10wt%) |

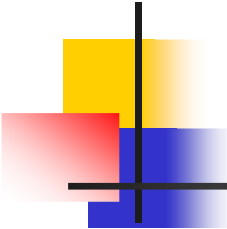


## Improvement in economical efficiency in conventional PWRs (2/2)

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### ADVANCED DESIGN FEATURES

- (1) Fuel pellet density : 95%TD → **97%TD**
- (2) Grid : Inconel → **Zircaloy**
- (3) Gadolinium content : 6wt% → **10wt%**
- (4) Advanced fuel cladding
- (5) **Debris filter** at bottom of fuel assembly



## Improvement of core design methodology and core management (1/2)

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- Nuclear Design Methodology

from 1D / 2D Calculation to **3D Calculation**

- Thermal Design Methodology

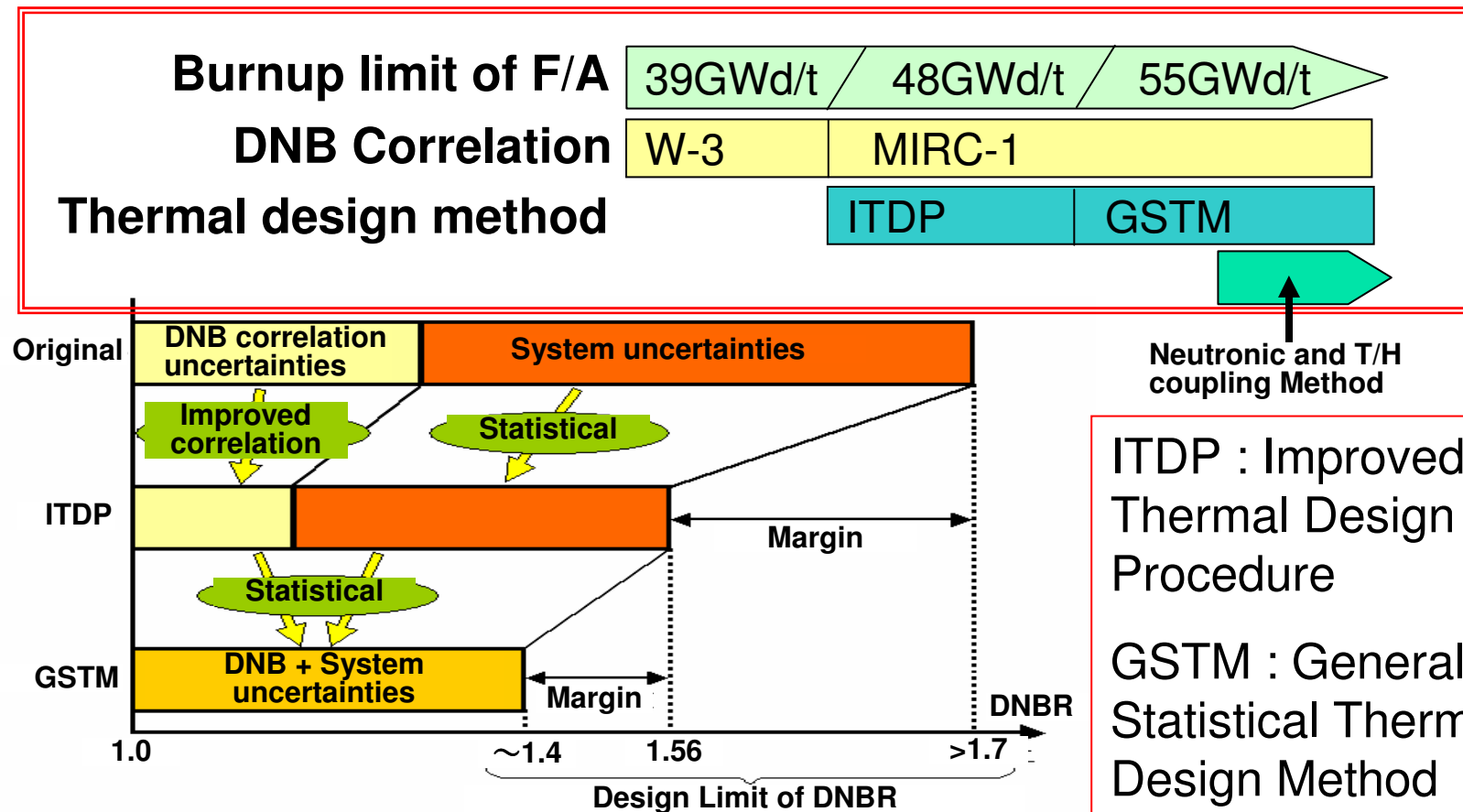
from ITDP to **GSTM**

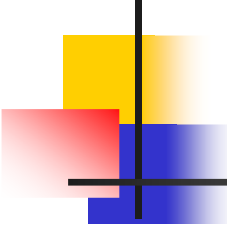
- Core Management

from M/D, NIS, T/C to **3D On-Line Core Monitor**  
(BEACON<sup>TM</sup>, GARDEL)

BEACON : Best Estimate Analyzer for Core Operation of Nuclear plants

# Improvement of core design methodology and core management (2/2)



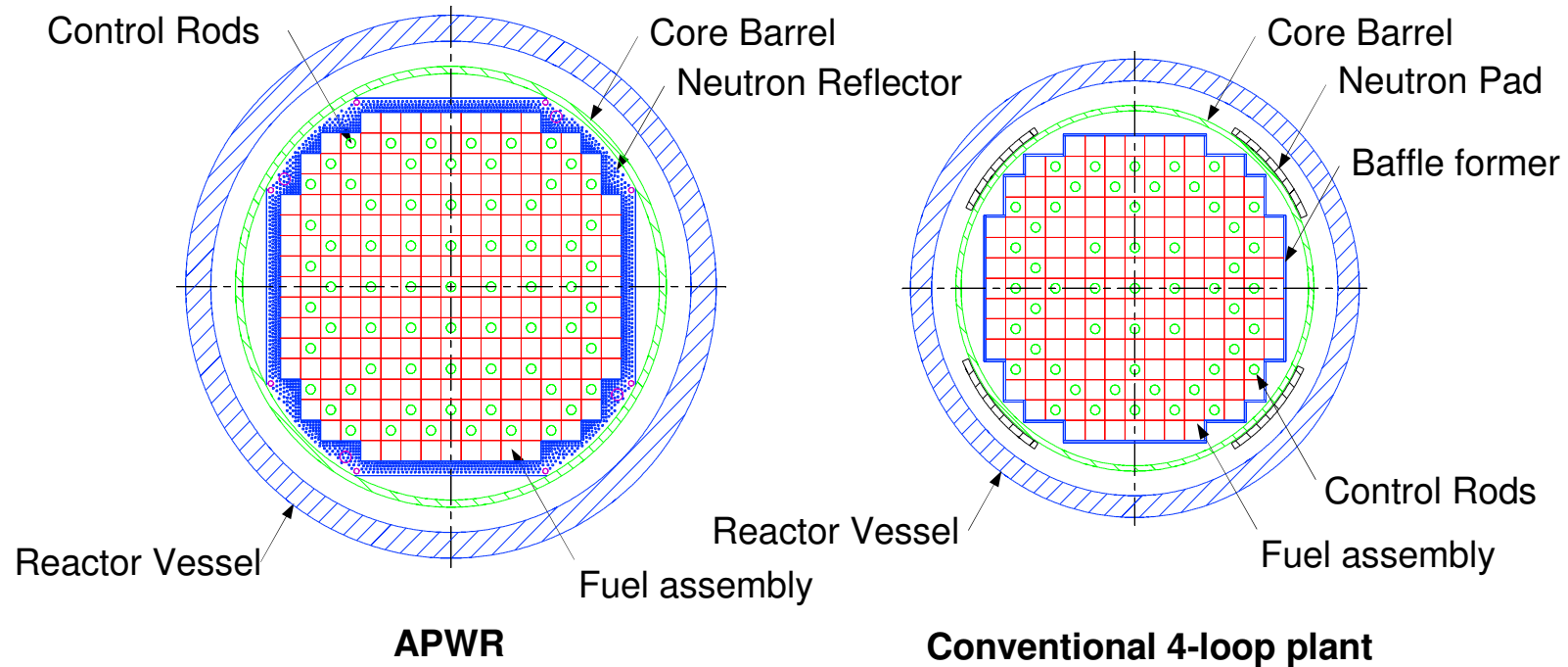


## Design Features of APWR core (1/2)

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- (1) Large Core : consists of 257 fuel assemblies of an advanced 17x17-type**
- (2) Fuel : has lower gas plenum with the advanced design features as mentioned before**
- (3) N/R : has radial neutron reflector**

## Design Features of APWR core (2/2)



## Comparison of Cores

# Nuclear Design Methodology(1)

## ■ 1D/2D Code System

- PANDA/LEOPARD/HIDRA (MHI)

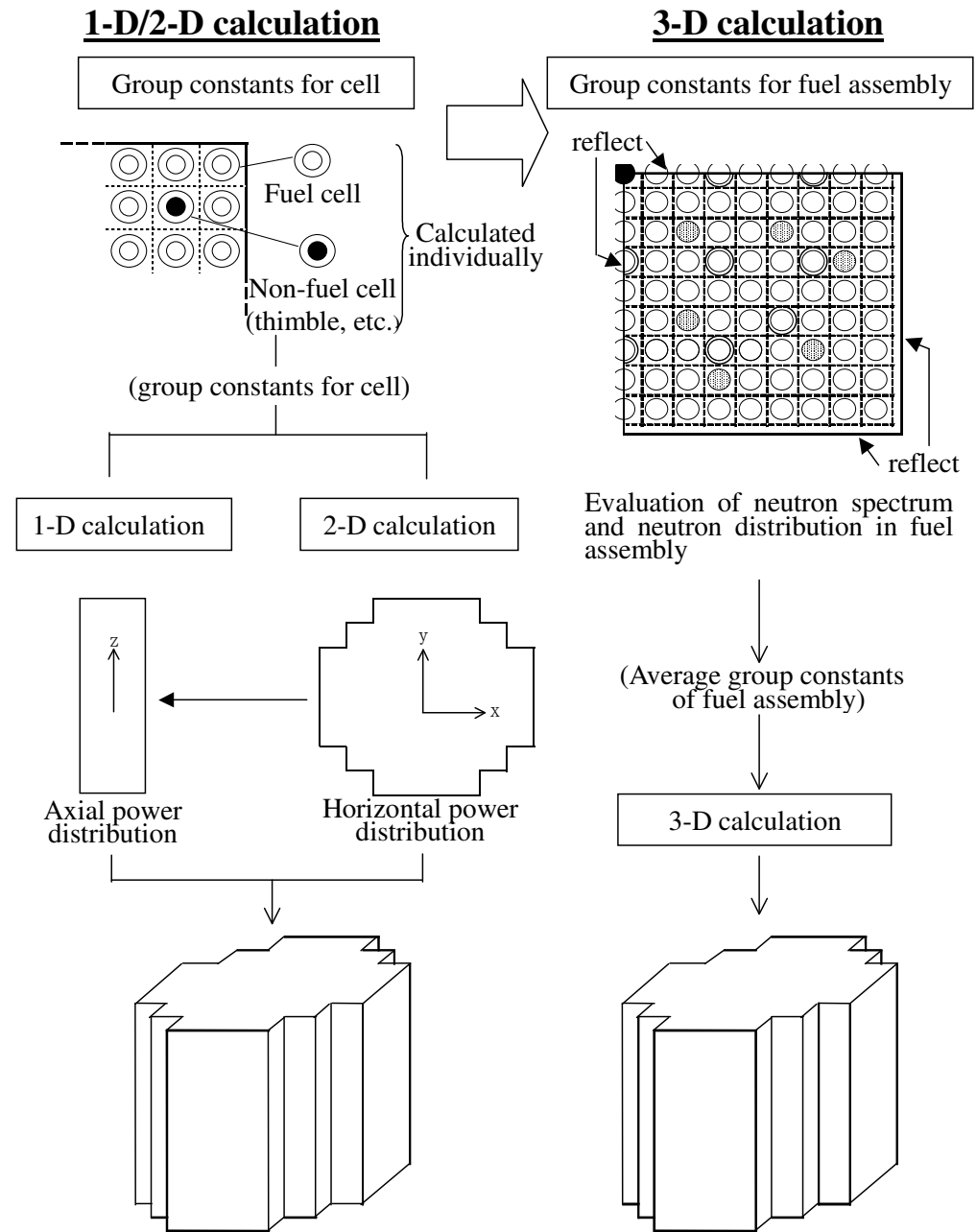
- NULIF/SHARP-A/  
SHARP-XY (NFI)

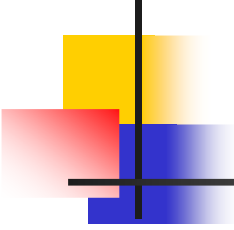
## ■ 3D Code System

- PHOENIX-P/ANC (MHI)

- Improved NULIF system (NFI)

- CASMO/SIMULATE (NEL)



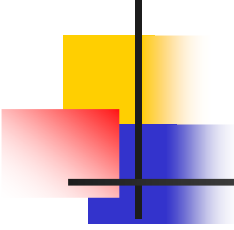


# Nuclear Design Methodology(2)

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## ■ **PHOENIX-P (MHI)**

- Generating 2-group constants to be used in core calculation
- Treating an single assembly or 4-assembly model with heterogeneity of fuel cells
- Employing transport theory (response matrix and  $S_N$ )
- Multi-group XS library

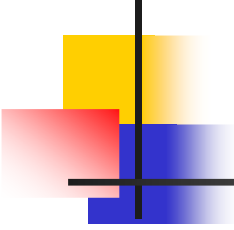


# Nuclear Design Methodology(3)

---

- **ANC (MHI)**

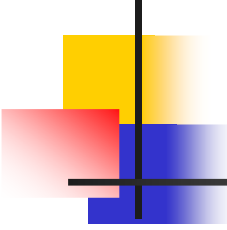
- Predicting PWR core performance parameters
- Employing Diffusion Nodal Expansion and pin power recovery method
- Nodal Expansion Method: Polynomial
- Pin power recovery: Group theory



# Nuclear Design Methodology(4)

---

- **Improved NULIF System (NFI)**
  - Generation of 2-group constants and Prediction of Core Performance
  - Spectrum interference effect by the Multi-assembly model
  - Pin power prediction by 2D pin-by-pin / 3D improved CM synthesis method
  - Improvements on burnup chain in the assembly calculation



# Nuclear Design Methodology(5)

---

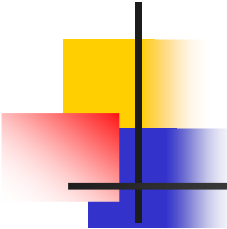
- **CASMO/SIMULATE (NEL)**

- CASMO

- Heterogeneous 2D transport calculation using the method of characteristics (MOC)
- Capability of performing full-core heterogeneous transport and depletion calculation

- SIMULATE

- Advanced nodal diffusion model
- MOX core analysis model
  - Semi-analytic nodal model
  - Nodal transport model
  - Spectral interaction model



# Improvement of design system for near future : MHI Case (1)

---

## [Cross section library]

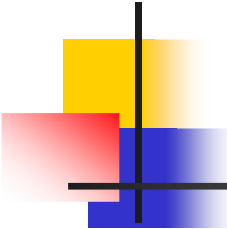
ENDF/B-V 42-group to **ENDF/B-VI 70-group**  
(**JENDL3.3 200-group** is under development)

## [Lattice Code]

Response Matrix &  $S_N$  to **CCCP**  
(PARAGON(**CCCP with DAF**) is ready to use.)

## [Core Calculation Code]

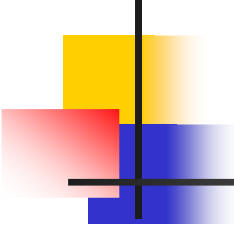
Nodal method to **Semi-analytical Nodal method**  
Group theory to **Fourier Transformation**  
Xe and Sm feedback to **micro-depletion method**  
4-assembly model to **single assembly with SPC**



## Improvement of design system for near future : MHI Case (2)

---

- **PARAGON**: New Lattice Physics Code developed by **MHI and Westinghouse**
  - Current Coupling Collision Probability with Discrete Angular Flux
  - Function to generate power profile within fuel rod by Spatially Dependent Dancoff Method (SDDM)
  - Full FORTRAN90 features.
    - Dynamic memory allocation etc..
    - Any number of space mesh and energy groups can be handled.



# Improvement of design system for near future : MHI Case (3)

---

## ■ PARAGON basic theory

**C**urrent **C**oupling **C**ollision **P**robability with **D**iscrete  
**A**ngular **F**lux equation

$$V_i \phi_i = \sum_{\alpha} \sum_{n,m} J_{-,\alpha}^{nm} P_{i,s_{\alpha}}^{nm} + \sum_j V_j F_j p_{ij}$$

$$J_{+,\alpha}^{nm} = \sum_{\beta} \sum_{k,\ell} J_{-,\alpha}^{k,\ell} P_{s_{\alpha},s_{\beta}}^{nm,k\ell} + \sum_j V_j F_j p_{s_{\alpha},i}^{nm}$$

$$J_{+,\alpha}^{nm} = \beta_{\alpha}^{nmk\ell} J_{-,\alpha}^{k\ell}$$

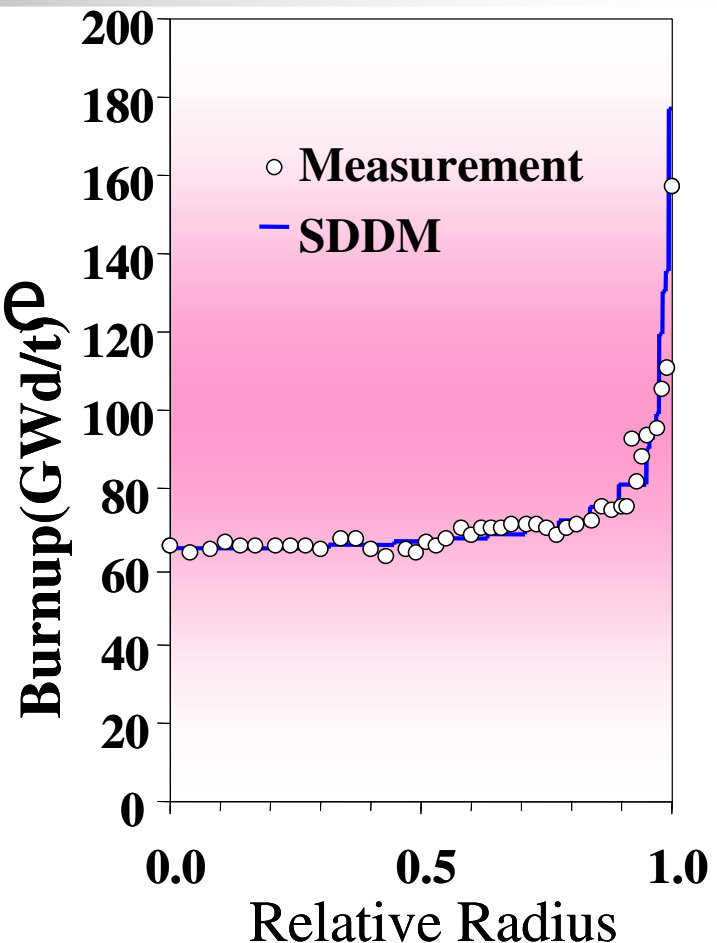
# Improvement of design system for near future : MHI Case (4)

## ■ Resonance XS

for Lattice code  
Spatially Dependent  
Dancoff Method(**SDDM**)  
was developed. (2002)

The method has been  
put in **PARAGON**

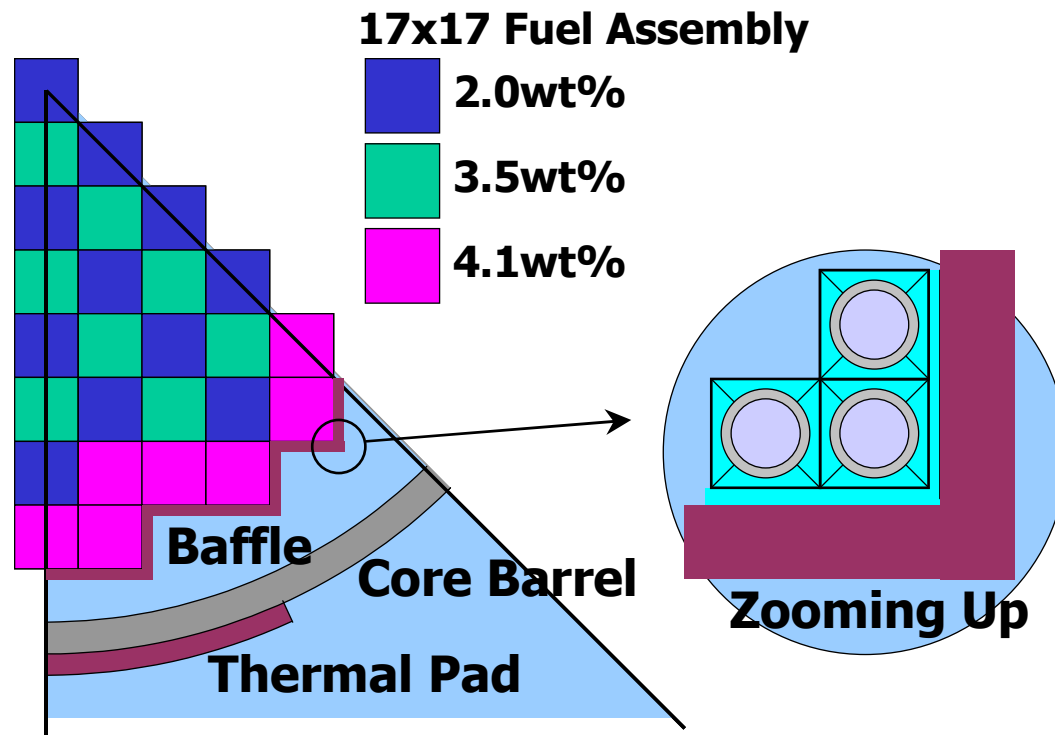
Measurement: CRIEPI



Burnup distribution within  
Fuel Rod(Average 74.5GWd/t)

# Improvement of design system for near future : MHI Case (5)

## ■ Large Scale Calculation



A Japanese typical 3loop initial Core

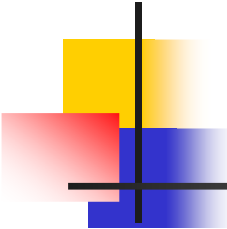
**K-eff**

**PARAGON: 0.9980**

**MCNP :0.9991(1 $\sigma$ 0.02%)**

|      |      |      |      |     |  |
|------|------|------|------|-----|--|
| -2.2 |      |      |      |     |  |
| -2.1 | -1.2 |      |      |     |  |
| -1.3 | -0.5 | -0.4 |      |     |  |
| -1.2 | -0.8 | -0.7 | -0.9 |     |  |
| -1.7 | 0.0  | -0.7 | 2.1  | 2.2 |  |
| -1.8 | -1.7 | 1.4  | 3.0  | 3.5 |  |
| -1.5 | 0.3  | 0.8  | 1.8  |     |  |
| -1.1 | -1.2 |      |      |     |  |

**Assembly Power Comp.**  
**(PARAGON-MCNP)/**  
**MCNP x 100(%)**



## Improvement of design system for near future : MHI Case (6)

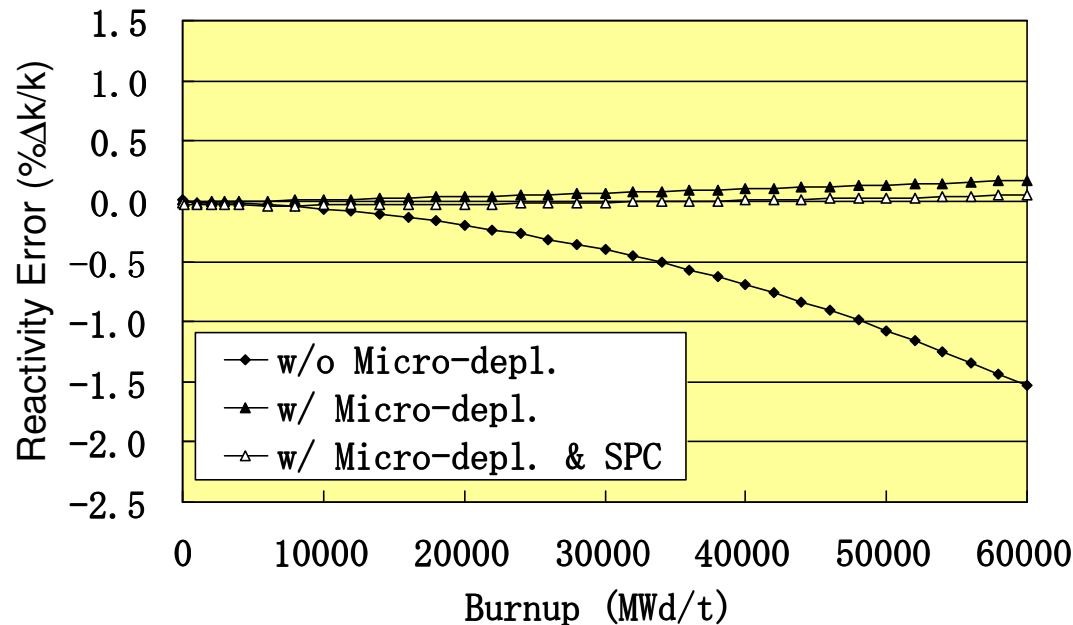
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### Core Calculation code for near future Micro-Depletion Correction Model

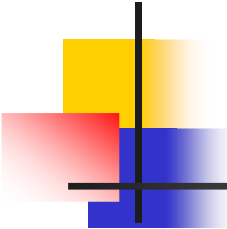
- **Explicit Tracking of Number Density**
    - Based on Two-Group Flux and Micro XS
    - Predictor-Corrector Method for Depletion (except for Gadolinia chain)
  - **Correction to Macro XS**
    - Determine the Difference of Contribution to the Macro XS
- $$\Delta \Sigma_{ag} = \sum_i \left( \sigma_{ag,i}^{actual} N_{i,actual} - \sigma_{ag,i}^{ref} N_{i,ref} \right)$$
- Applied to Absorption and Fission XS

## Improvement of design system for near future : MHI Case (7)

- Reactivity Error with Spectral Correction  
(Relative Power=1.0, **Boron=1000ppm**)



Two-group constants were generated with PHOENIX-P where 1.0 power and **500ppm** boron were assumed.



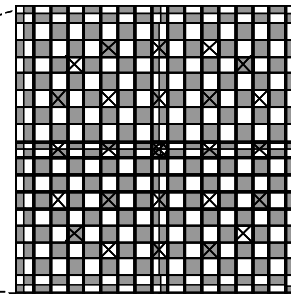
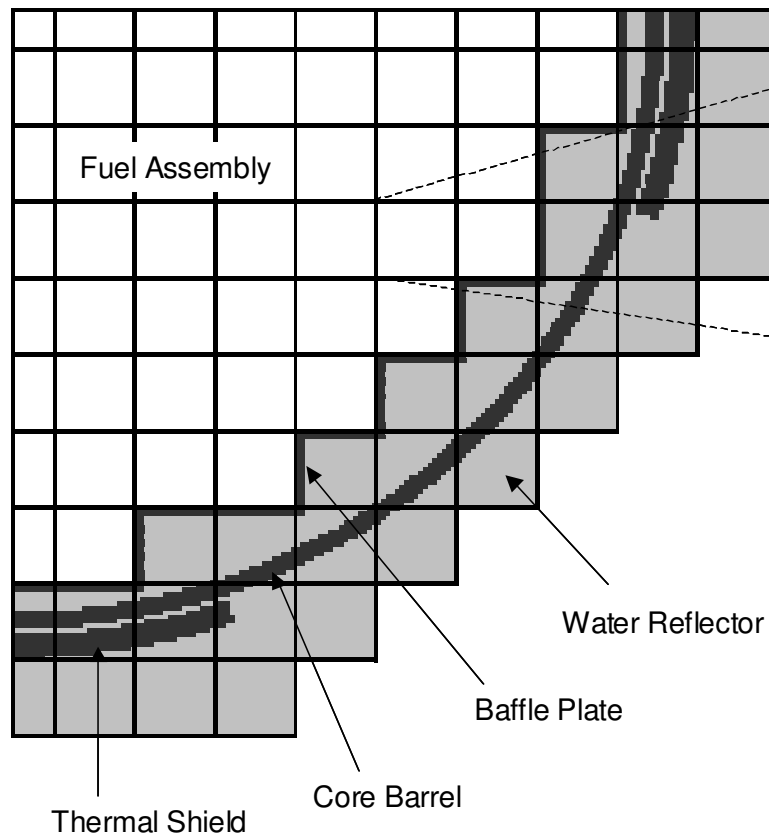
# Improvement of design system for near future : NFI Case (1)

---

- **SCOPE2**: PWR Core Calculation Code for the Next Generation Developed by **NFI**
  - One of the most precise method ever
    - 3-D Pin-by-Pin geometry
    - Multi-group (currently 9 groups)
    - Nodal SP3 transport theory method
  - Fully featured for reload core design
    - Reloading, grid treatment, RCC cusping, etc.
  - Realistic computing time for depletion calc.
    - ~2.5 hours by 24 processors (P-4 2GHz)

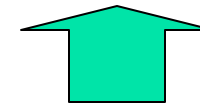
# Improvement of design system for near future : NFI Case (2)

## ■ 3-Dimensional Pin-by-Pin Geometry



Each assembly has  
20x20 fine meshes  
in the Red/Black  
coloring scheme.

Pin-cell averaged XS



Correction Factor  
By

**Improved-SPH method**

| Total Mesh Numbers | Total Memory |
|--------------------|--------------|
| 340 x 340 x 26     | Approx. 5GB  |

# Improvement of design system for near future : NFI Case (3)

## 3-Loop Type PWR HZP Power Distribution by SCOPE2

### Initial Core

|    | H    | G    | F           | E    | D    | C    | B   | A   |
|----|------|------|-------------|------|------|------|-----|-----|
| 8  | 0.3  | 0.1  | -0.2        | -0.6 | -0.8 | -0.4 | 0.2 | 0.7 |
| 9  | -0.1 | -0.3 | -0.4        | -0.5 | -0.7 | -0.3 | 0.0 | 0.7 |
| 10 | -0.4 | -0.5 | 0.0         | -0.1 | 0.0  | 0.0  | 0.4 |     |
| 11 | -1.0 | -0.9 | -0.3        | 0.1  | 0.0  | 0.3  | 0.6 |     |
| 12 | -1.0 | -0.9 | -0.1        | 0.3  | 0.4  | 0.6  |     |     |
| 13 | -0.6 | -0.6 | 0.1         | 0.4  | 0.6  |      |     |     |
| 14 | 0.3  | 0.1  | 0.7         | 0.5  |      |      |     |     |
| 15 | 1.1  | 1.1  | -- Error[%] |      |      |      |     |     |

**RMS=0.5%**  
**MAX=1.1%**

### Reload Core

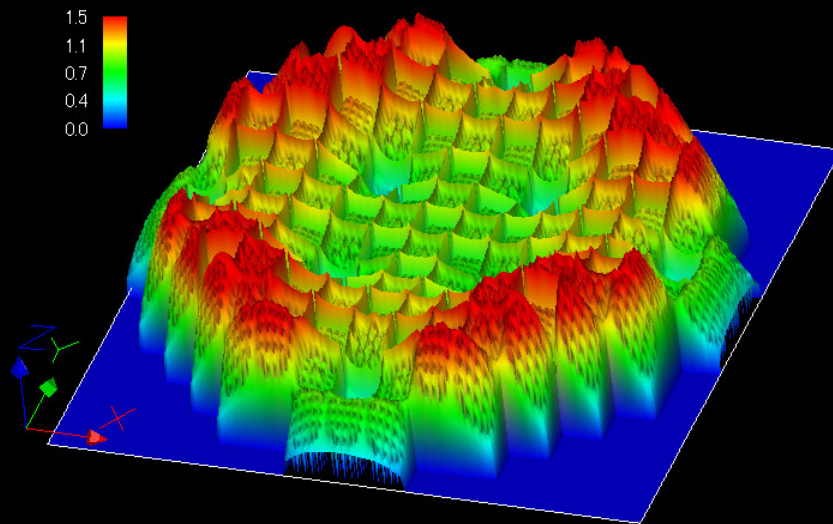
|    | H    | G    | F           | E    | D    | C    | B   | A   |
|----|------|------|-------------|------|------|------|-----|-----|
| 8  | 0.2  | 0.6  | 0.0         | -0.1 | 0.1  | 0.7  | 0.6 | 0.3 |
| 9  | 0.8  | 1.0  | 0.7         | 0.5  | 0.3  | 0.7  | 0.6 | 0.1 |
| 10 | 0.3  | 0.6  | -0.6        | -1.3 | -1.6 | 0.2  | 0.6 |     |
| 11 | 0.9  | 1.0  | -0.9        | -1.5 | -1.3 | 0.4  | 0.4 |     |
| 12 | 0.8  | 1.0  | -1.5        | -1.7 | -1.6 | -0.3 |     |     |
| 13 | 1.2  | 1.1  | 0.1         | 0.6  | -0.1 |      |     |     |
| 14 | 0.1  | 0.1  | -0.8        | 0.2  |      |      |     |     |
| 15 | -0.6 | -0.7 | -- Error[%] |      |      |      |     |     |

**RMS= 0.9%**  
**MAX=-1.7%**

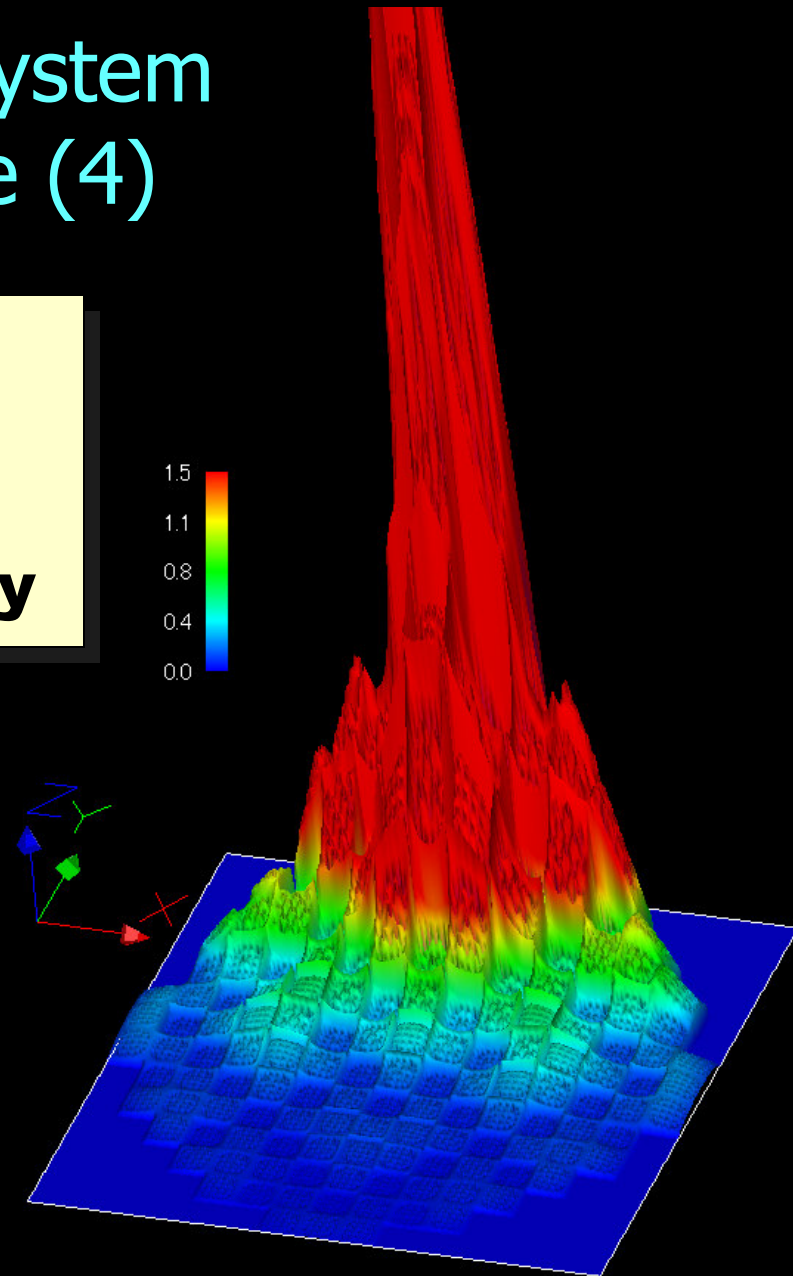
\* Error=(Meas.-SCOPE2)/SCOPE2×100(%)

# Improvement of design system for near future : NFI Case (4)

**3-Loop Type Initial Core  
HZP Power Distribution  
by **SCOPE2**  
in 3-D Pin-by-Pin Geometry**



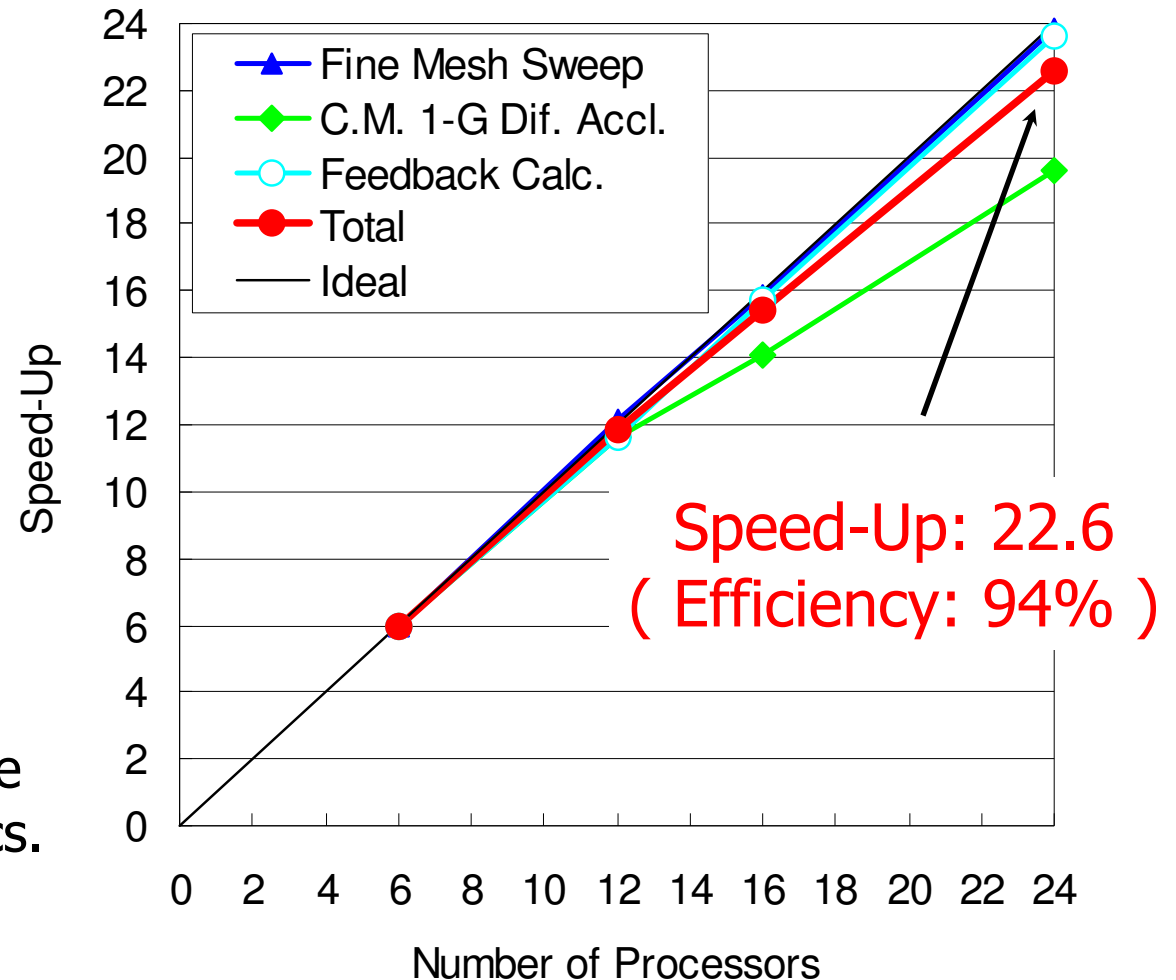
**RCC D-Bank In**



**All-Rods-In with 1-Rod Stuck**

# Improvement of design system for near future : NFI Case (5)

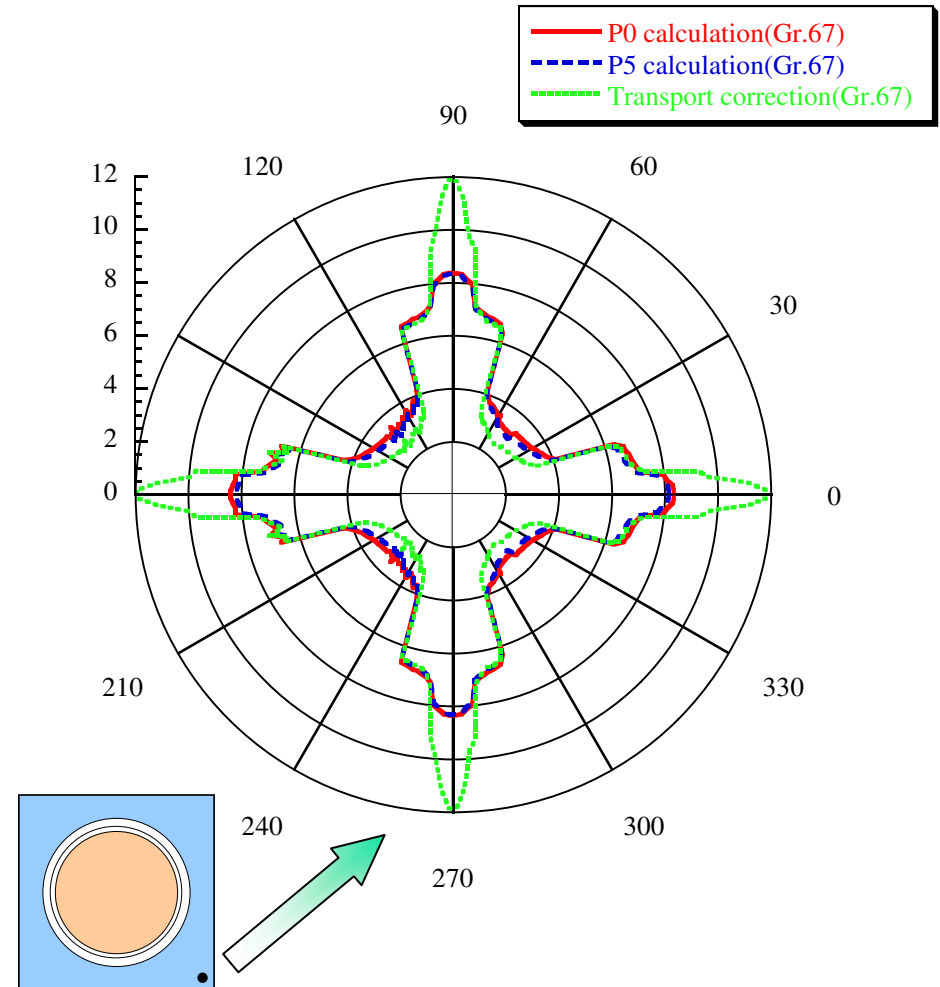
- Identical Results in Parallel Computing
  - Important in view of quality assurance for design calculations
  - Fine-grained Parallel Algorithm
- Good Scalability
  - Enough for middle-size cluster with  $\sim 24$  procs.



# Improvement of design system for near future : NEL Case (1)

## ■ **NELAT: Rigorous Lattice Physics Code for the Next Generation Developed by NEL**

- Heterogeneous 2D Transport Calculation based on the Characteristics Method
- Efficient Ray Tracing using the Macroband Method
- Efficient Angular Integration Scheme using the Polynomial Expansion for Neutron Flux
- Capability of Treating the Anisotropic Scattering Source Up to  $P_5$  Order



**Angular Flux Distribution  
(12wt%Pu<sup>tot</sup> MOX Fuel Cell)**

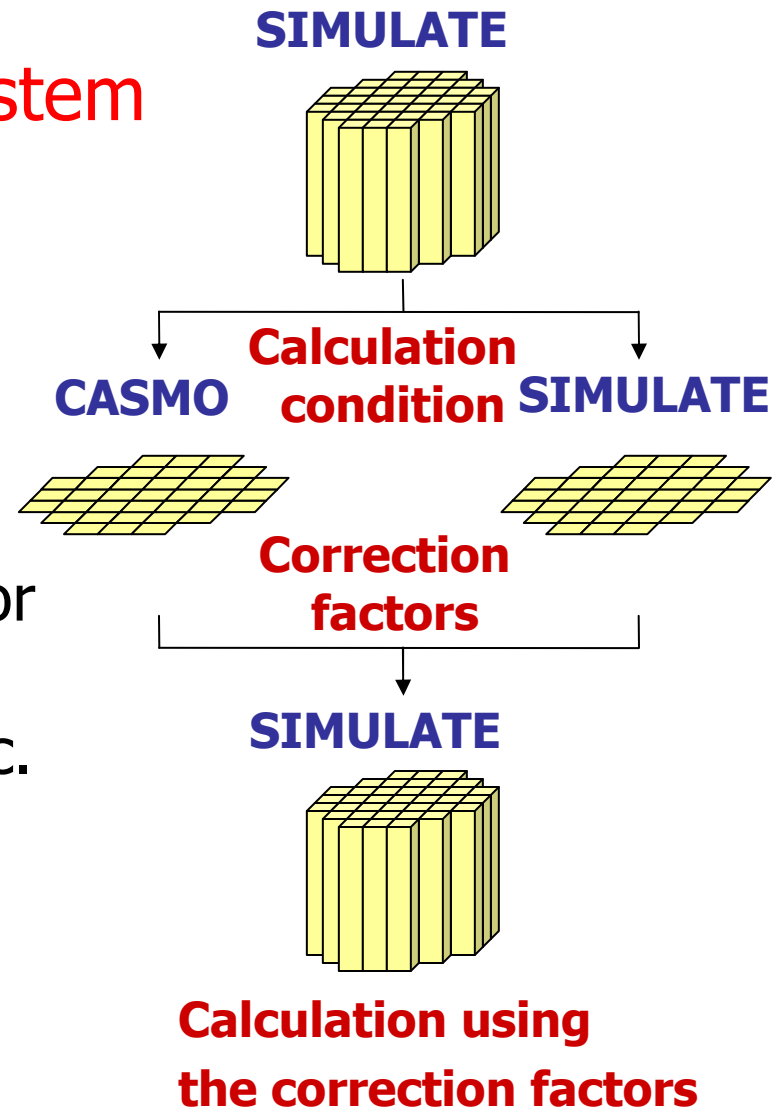
# Improvement of design system for near future : NEL Case (2)

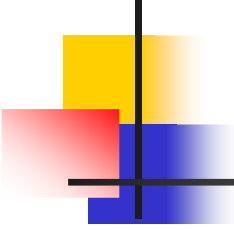
## Hybrid Core Calculation System

Compare the CASMO and SIMULATE *2-D* core calculation results under the predetermined *consistent* calculation condition

Generate the *correction factors* for assembly homogenized cross sections, discontinuity factors, etc.

Apply them for SIMULATE 3-D calculation

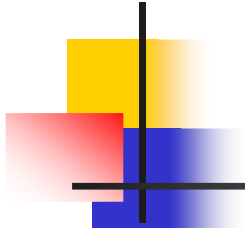




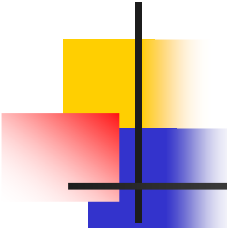
## 4. FR Analysis Codes

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- Cell Codes
  - SLAROM,
  - CASUP
- Core Calculation Codes
  - CITATION
  - TRITAC(XYZ)
    - DSA
    - JUPITER
  - NSHEX
    - Nodal Transport in Hex.-z



- Detailed Core Calculation  
BACH---MOC+Axial Leakage 3D (Hex-z)
- Sensitivity Codes  
SAGEP---2D, 3D  
---GPT(Generalized Perturbation Theory Based  
on Diffusion Theory)  
SAINT---1D, 2D  
Sensitivity in Cells and Assemblies, GPT Based on  
FFCP  
ABLE  
Cross Section Adjustment with Method Uncertainty



# Calculation Flow of BACH

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CASUP

Calculate effective macro cross section



MOC code for hexagonal geometry

Calculate intersection between Pass line and geometry and length of the segment

Correct the width of Pass line so that each area is kept constant

Calculate the angular flux along Pass line

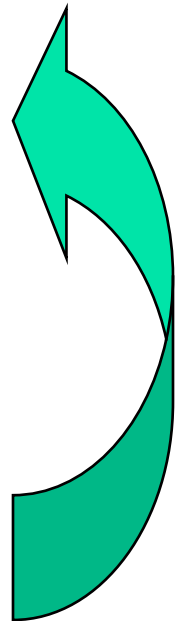
Calculate the scalar flux



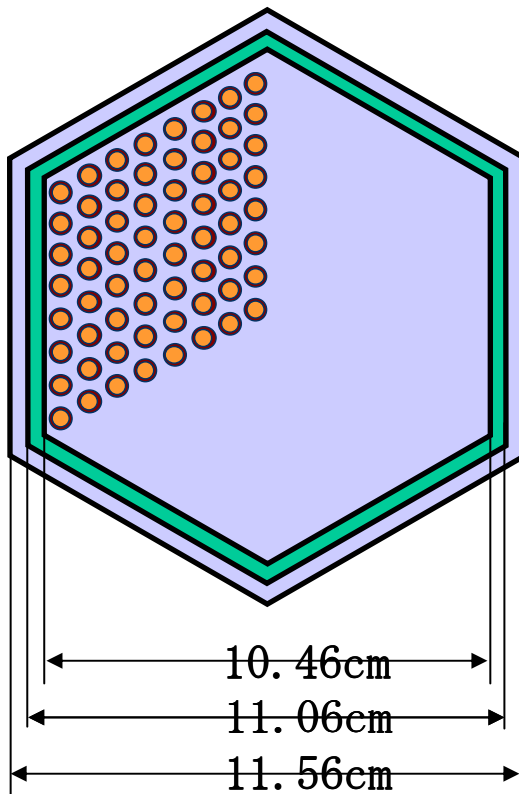
Make homogenized macro cross section

HEX-Z nodal transport code

Calculate axial leakage and power distribution



# Infinite assembly problem



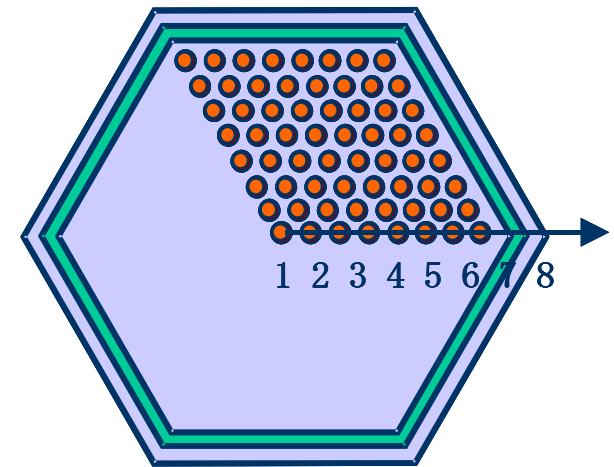
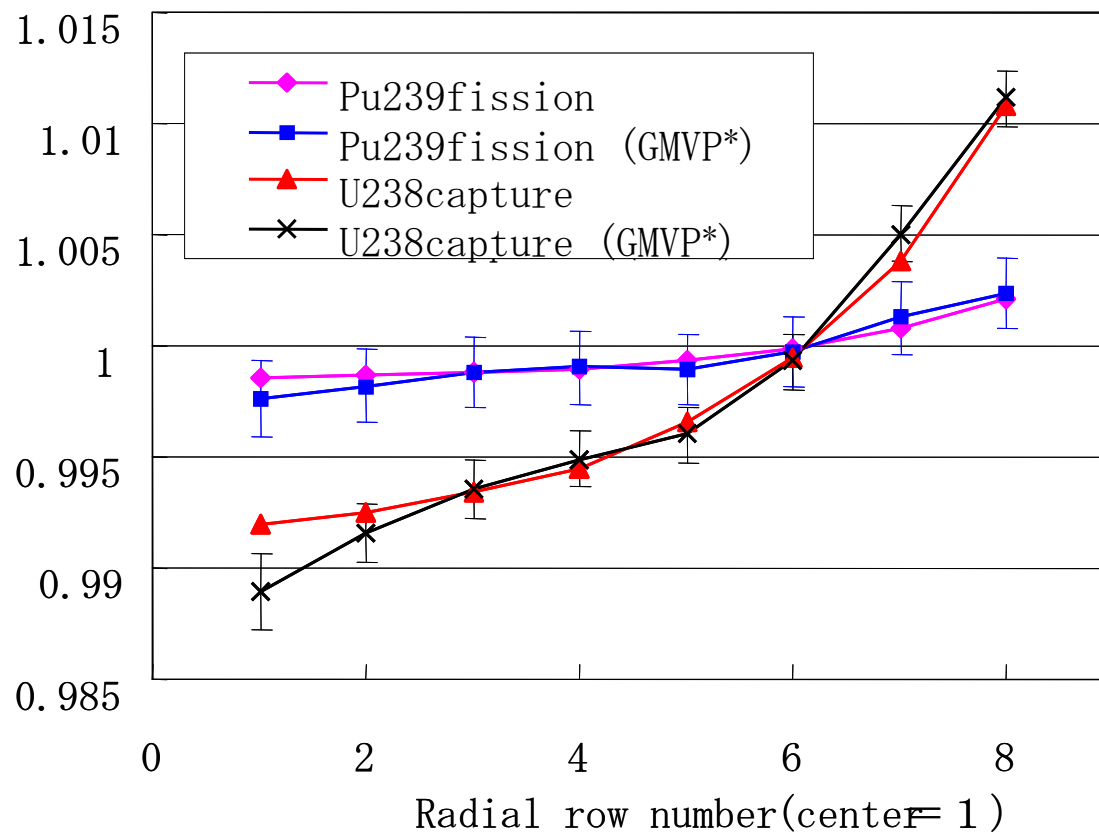
Calculation Model

| Fuel Rod             |           |
|----------------------|-----------|
| Number               | 169       |
| Diameter of Fuel     | 0.54 c m  |
| Diameter of Cladding | 0.65 c m  |
| Pin Pitch            | 0.787 c m |

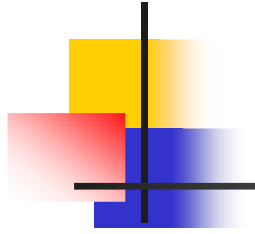
## Material

|                         |           |
|-------------------------|-----------|
| Fuel                    | MOX       |
| Cladding & Wrapper Tube | Stainless |
| Coolant                 | Na        |

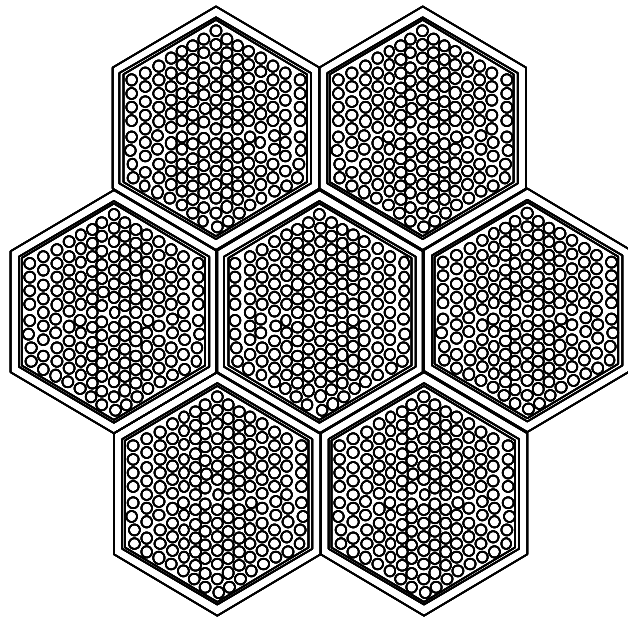
# Reaction rate distributions



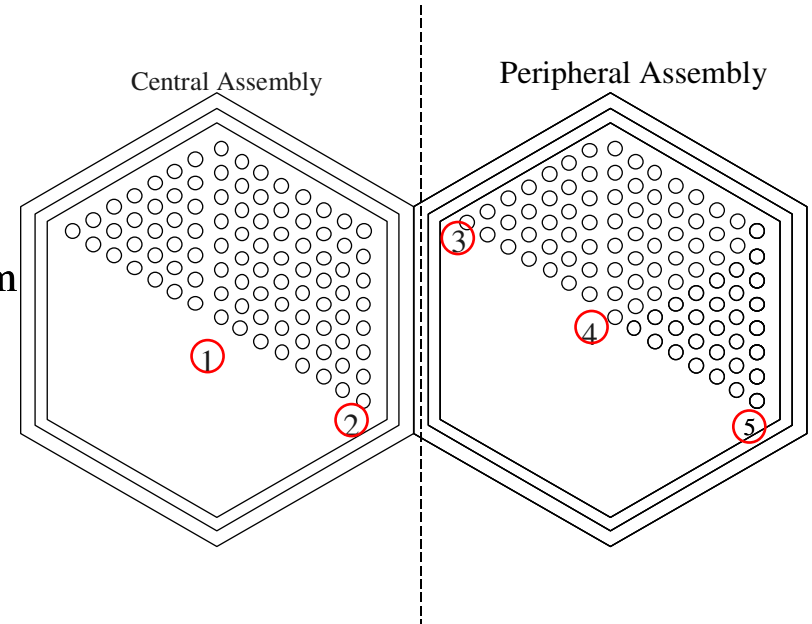
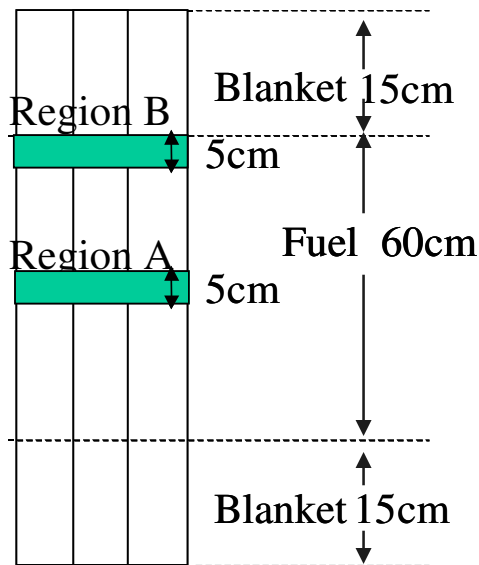
\* GMVP: Monte-Carlo code



# 3D Calculation



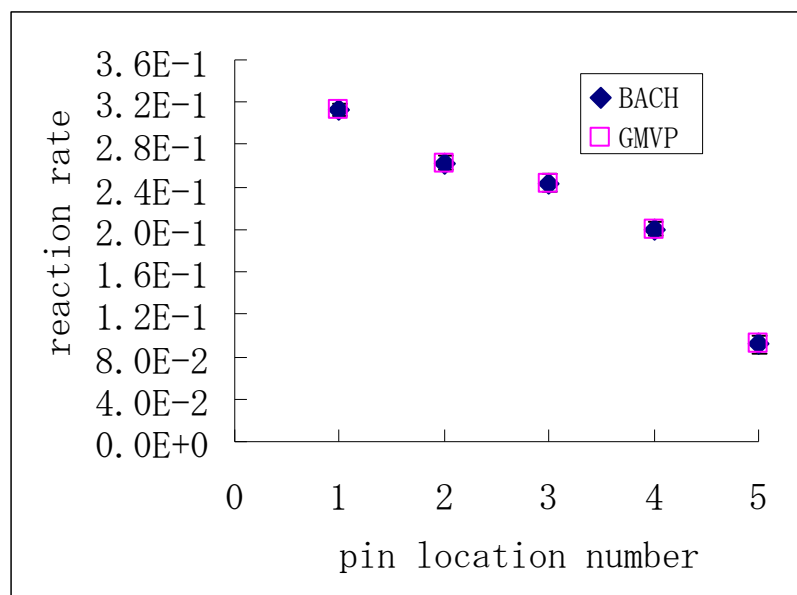
Boundary:vacuum



Calculation Model

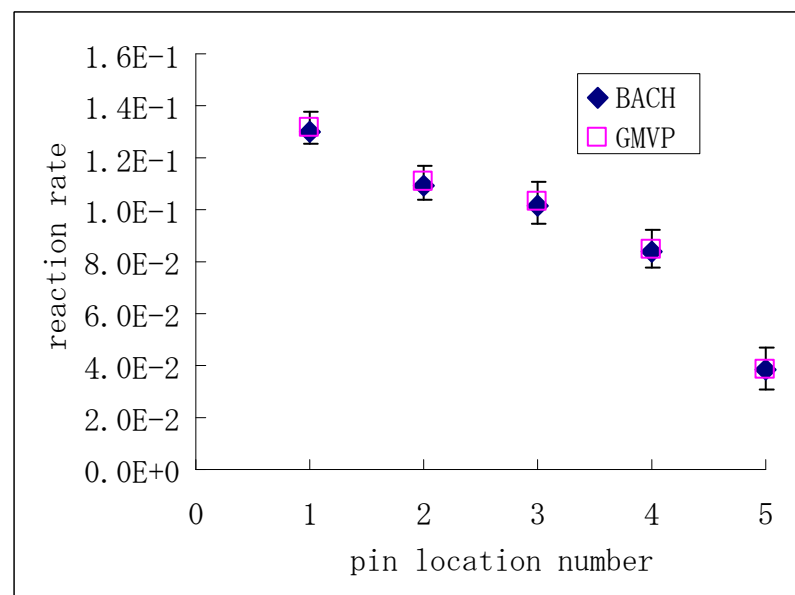
# Reaction rate in individual pins

Np-237 Capture



Region A

GMVP: 5000\*10000 history



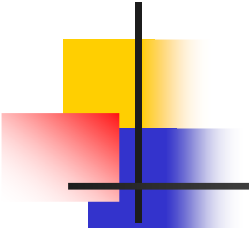
Region B



# JNC Activities

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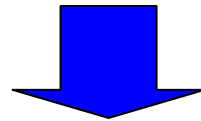
- Development of SLAROM-UF
- Covariance Processing Code : ERRORJ
- Reactor Constant Adjustment
- Programme of PIE Analysis at JNC
- NGSC (Next Generation Simulation Code) in JNC



## Development of SLAROM-UF

---

- To improve the treatment of the resonance self-shielding in a heterogeneous cell
- To improve the treatment of the resonance self-shielding, and interaction between different nuclides , regions, and temperatures
- To apply various fast reactor core analyses for the feasibility study in JNC (Coolant/Fuel) **Na/MOX**, **Pb-Bi/MN**, **Gas/MN** reactor, etc.

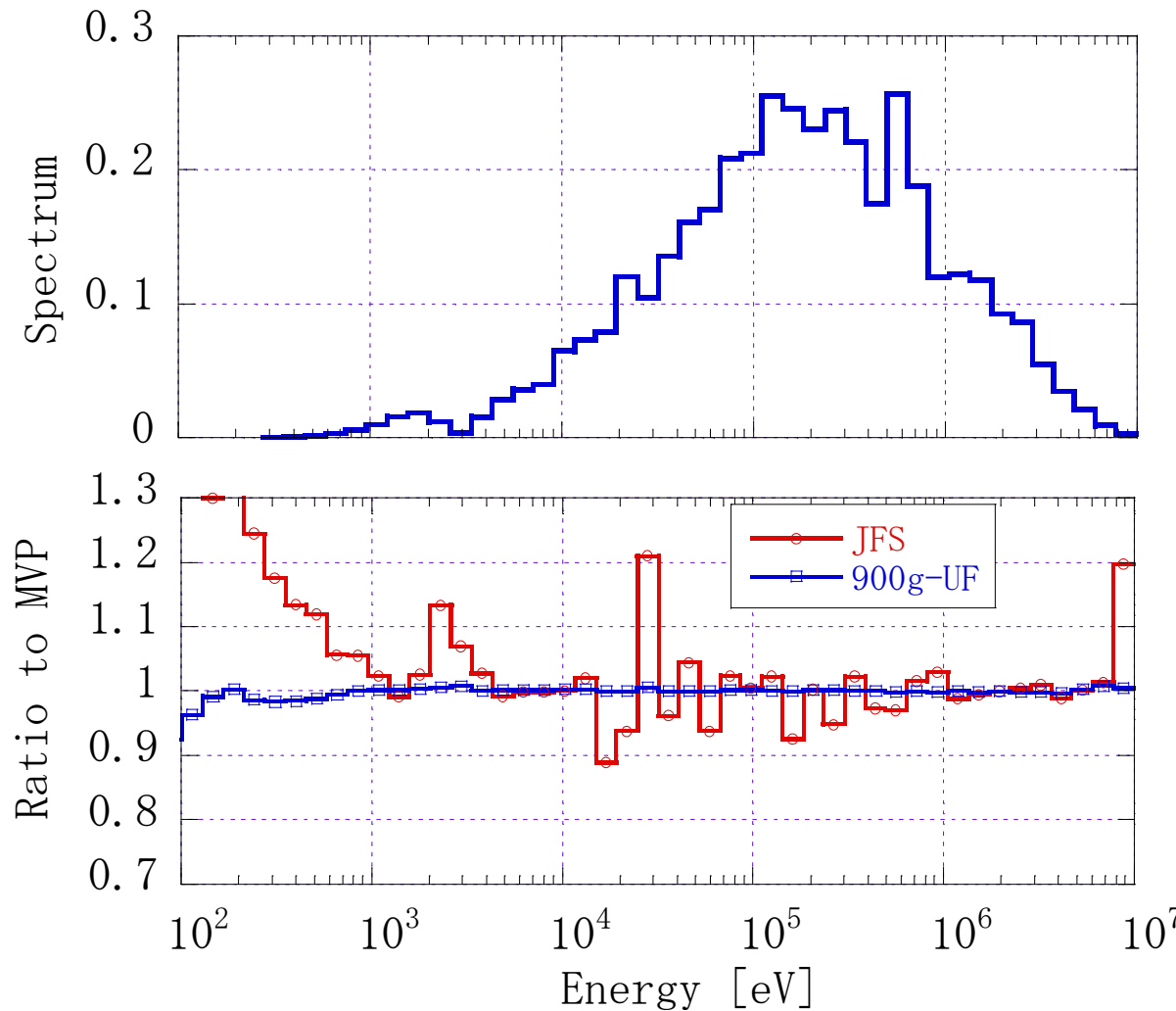


Developed new cell calculation code “SLAROM-UF”

Combination use of

- Slowing down equation in ultra fine (100,000) group structure  
for < 50keV
- Pij calculation in 900-group structure  
 $\Delta u=0.008$  for > 50keV (comparable to the ECCO 1,968-group library)  
Reflect ultra fine calculation result for < 50keV

# Application of SLAROM-UF

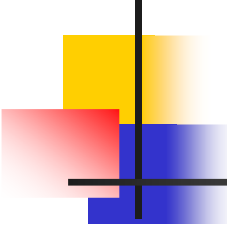


JOYO sub-assembly  
Infinite cell spectrum

Ratio to MVP

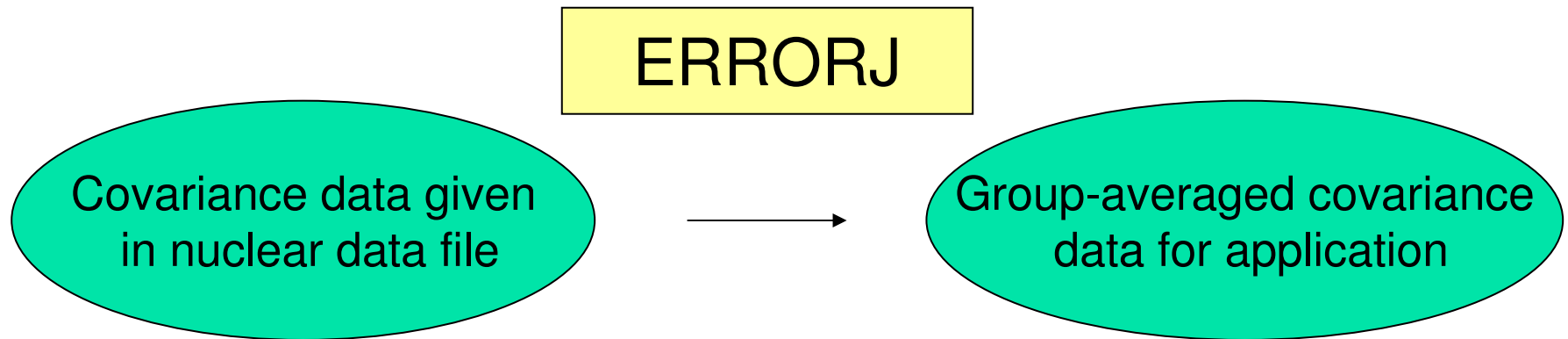
JFS : 70 group constant  
with f-table  
900g-UF : new result

Neutron spectrum by SLAROM-UF coincides with that by  
continuous energy Monte Carlo method.



# Covariance Processing Code:ERRORJ

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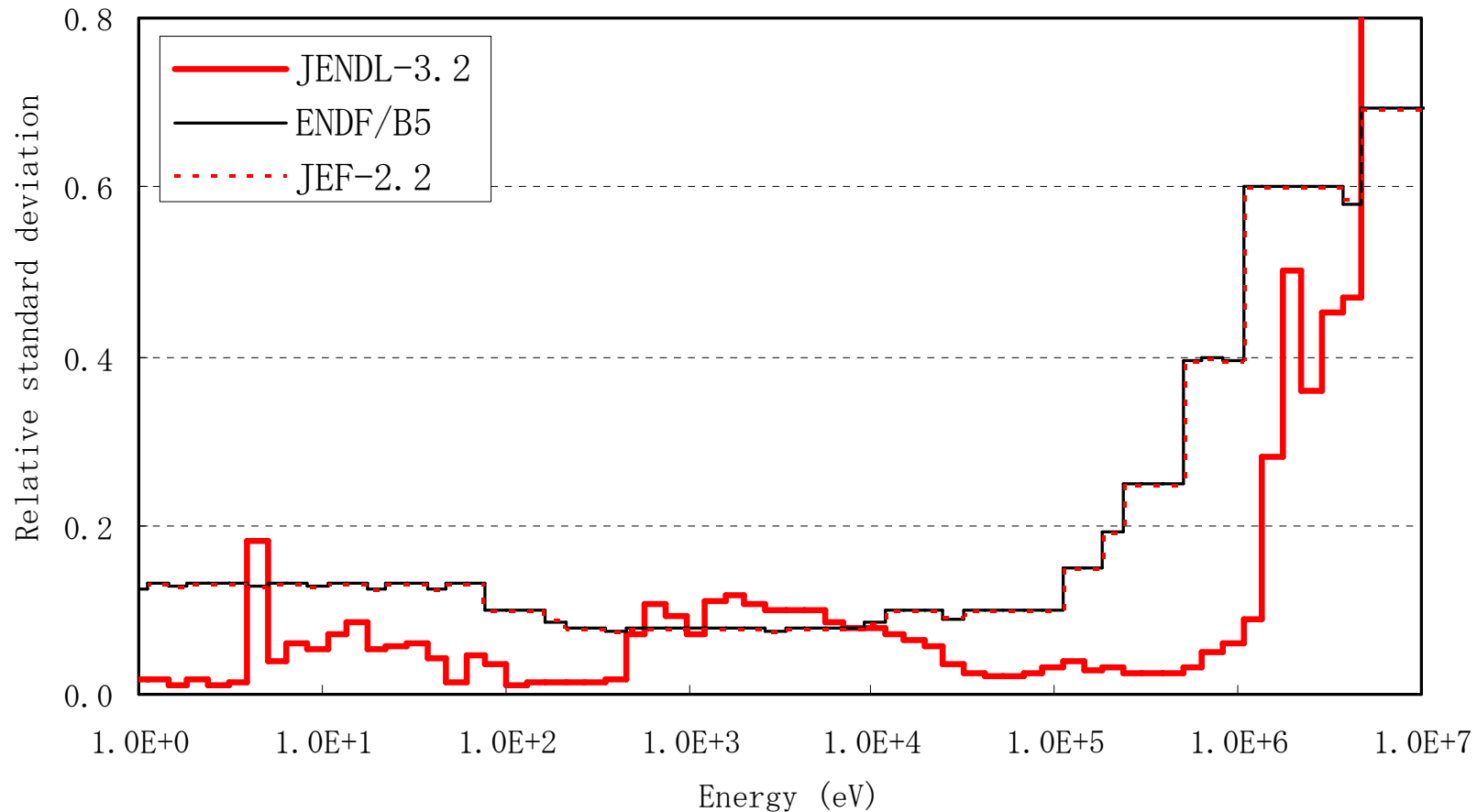


- Expanded processing for covariance of resonance parameters

Sensitivity coefficient of group constant to resonance parameter is calculated numerically.

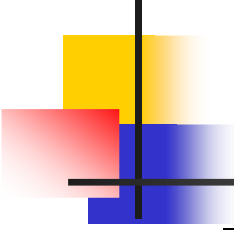
- Processing for  $\mu$  **and fission spectrum**

# Comparison of Covariance:U-235(n, $\gamma$ )



Uncertainty in criticality of BFS-62-1 core ( $1\sigma$ )

**340 pcm** (JENDL-3.2) **800 pcm** (ENDF/B-V)

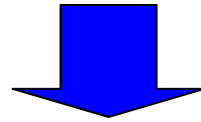


# Reactor Constant Adjustment

---

■ **ADJ2000R** has been used in the feasibility study

- Adjust JFS 70g constant based on **Bayesian theory**
- Use various experimental data of small to large Na-MOX core including **burn-up** and **temperature** related reactivity
- Use covariance data consistent with JENDL-3.2



Apply the adjustment technique to uncertainty evaluation  
of BN-600 hybrid core analysis with BFS-62 experiment

Confirm effectiveness of the technique

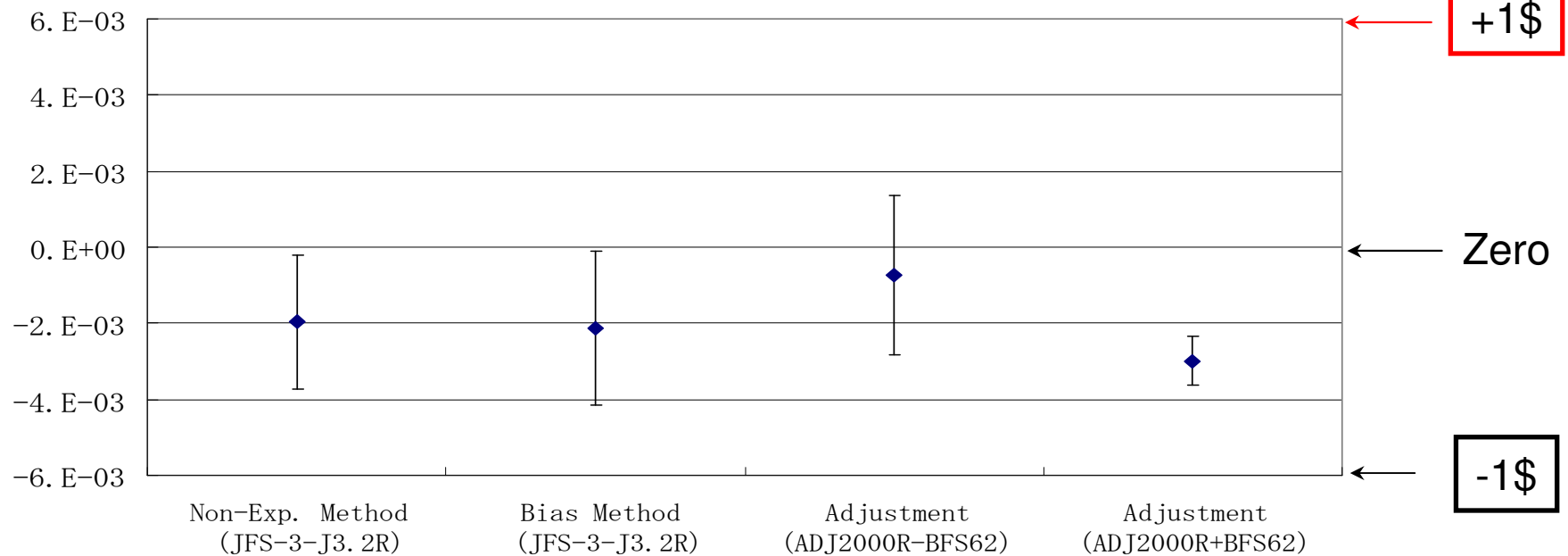
- (1) No-Information method (No experimental data is considered.)
- (2) E/C Bias Method = “Bias factor method”
- (3) Cross-Section Adjustment Method

Not considering BFS-62 data = “ADJ2000R - BFS62”

Considering BFS-62 data = “ADJ2000R + BFS62”

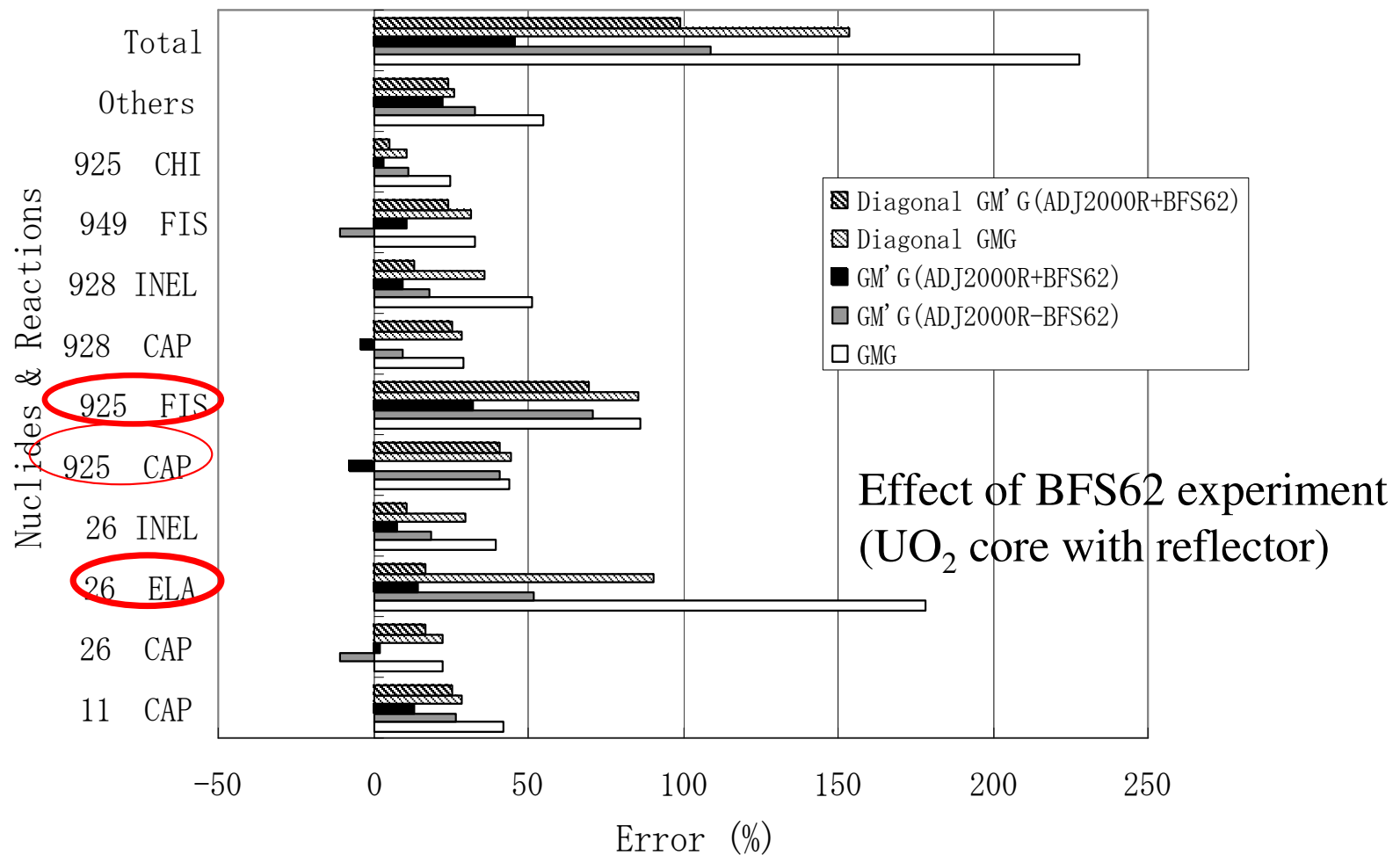
# Predicted Uncertainty on Sodium Void Reactiv:

(%dk/kk' )



|                                    |           |           |           |           |
|------------------------------------|-----------|-----------|-----------|-----------|
| Uncertainty ( $\phi$ )             | <b>30</b> | <b>34</b> | <b>36</b> | <b>11</b> |
| X-section-induced error ( $\phi$ ) | 27        | 31        | 25        | 5         |

# Breakdown of the Predicted Uncertainty



## Programme of PIE Analysis at JNC

- JOYO MK-I core fuel
- JOYO MK-II driver fuel
- MA samples irradiated at JOYO MK-II core

### MA sample irradiation

$^{237}\text{Np}$ ,  $^{241}\text{Am}$ ,  $^{243}\text{Am}$ ,  $^{244}\text{Cm}$

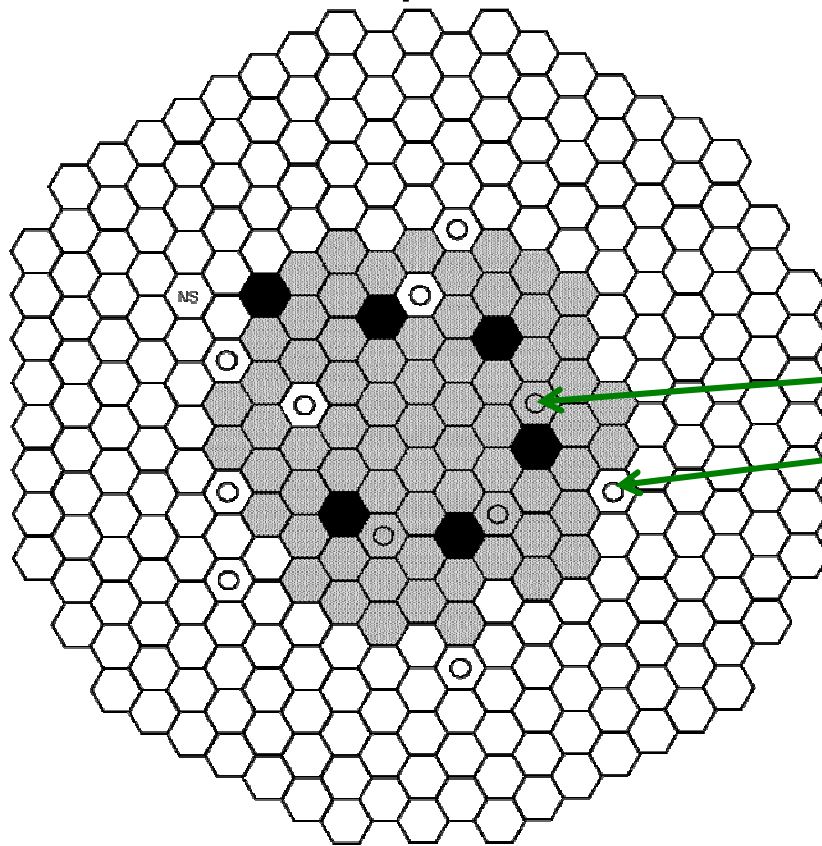
(Fourteen samples are in a PIE stage.)

### **Irradiation positions**

3<sup>rd</sup> row, 208 efpd (29<sup>th</sup>-32<sup>nd</sup> cycle)

5<sup>th</sup> row, 251 efpd (30<sup>th</sup>-33<sup>rd</sup> cycle)

Neutron flux:  $1 \sim 3 \times 10^{15} \text{ n/cm}^2 \text{ sec}$



**JOYO MK-II core (32<sup>nd</sup> cycle)**



Driver fuel



Control rod

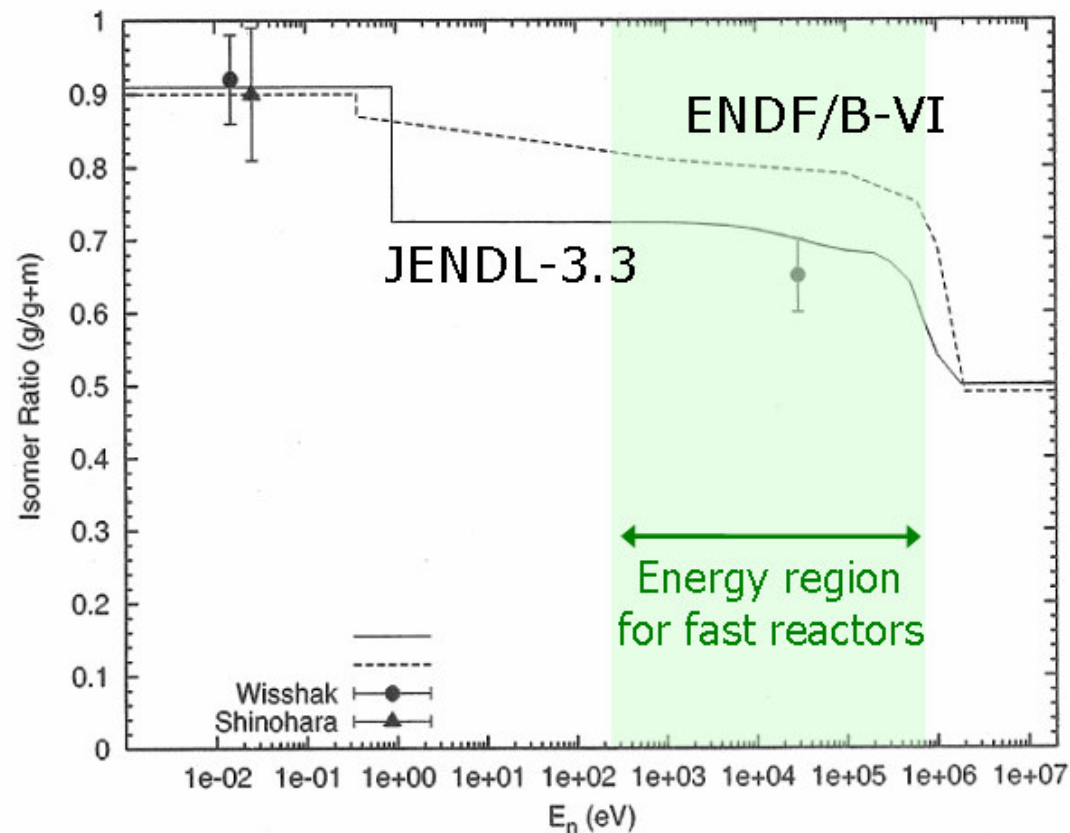


Irradiation test S/A



Reflector

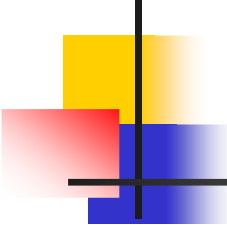
# Preliminary C/E Values on $^{242\text{m}}\text{Am} / ^{241}\text{Am}$ Abundance Ratio



Present status of the isomeric ratio for  $^{241}\text{Am}$  capture reaction

| Nuclear Data Library | $^{241}\text{Am}$ Isomer Ratio | C/E on $^{242\text{m}}\text{Am} / ^{241}\text{Am}$ |
|----------------------|--------------------------------|----------------------------------------------------|
| JENDL-3.2            | 0.80                           | 1.30                                               |
| JENDL-3.2            | 0.85                           | 1.00                                               |
| JENDL-3.3            | 0.85                           | 1.02                                               |
| ENDF/B-VI            | 0.85                           | 0.94                                               |
| JEF-2.2              | 0.85                           | 1.03                                               |

The above results implied the possibility that the  $^{241}\text{Am}$  isomeric ratio lies around **0.85**.



# NGSC (Next Generation Simulation Code) in JN

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## **Background**

- In 2002, feasibility study on computer technologies in support of NGSC concept was started inside JNC.
- In 2003, an expert group was set up in each of CEA and JNC to discuss jointly the development direction of future simulation codes and to put together a common report.

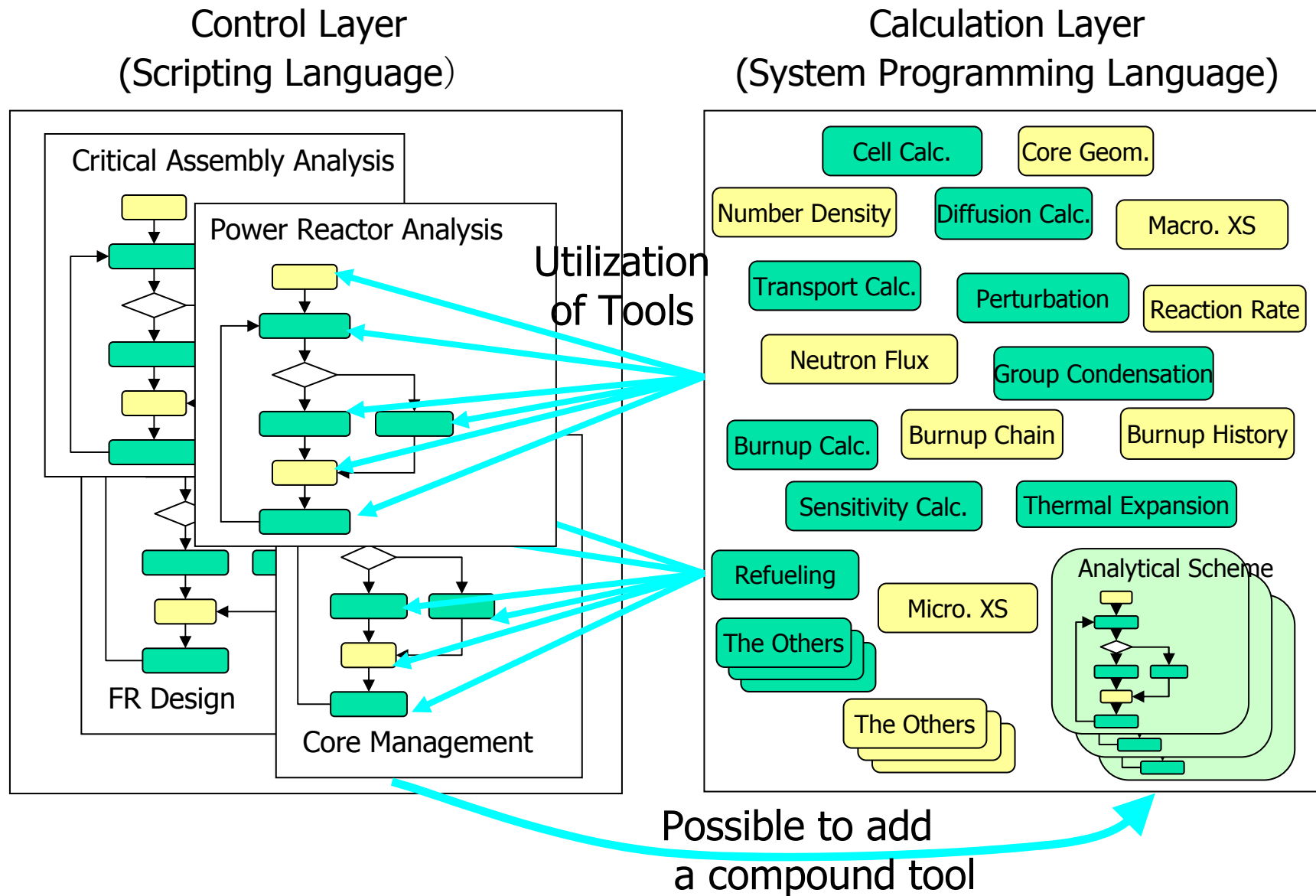
## **Needs**

- Development of advanced physics models
- Improvement of numerical solution methods and procedures
- Simulation methods for multi-physics phenomena
- Code validation by experiments

## **Main points of concept**

- Existing software properties or legacy codes are to be efficiently utilized (efficiency)
- De facto standard (universality) and accessible by engineers and researchers in nuclear societies (openness)
- Flexible and expandable (expansibility)
- Validation and qualification of the system (completeness)

# Architecture of NGSC for Reactor Physics



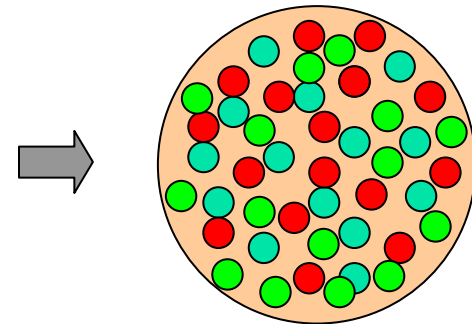
# 5. General Analysis Codes

MVP: general purpose Monte Carlo code based on the continuous-energy model

- Time-dependent neutron and photon transport problems
- External-source and fission-source ( $k_{eff}$ ) problems

## Features

- Fast computation algorithm for vector and/or parallel computers
- Arbitrary temperature calculation  
(Internal production of temperature dependent libraries)
- Burn-up calculation
- **Statistical geometry model**  
for randomly distributed lots of particles  
(analyses of HTGR, plutonium spots etc.)
- Accurate perturbation calculation
- Noise analysis (Feynman- $\alpha$ )



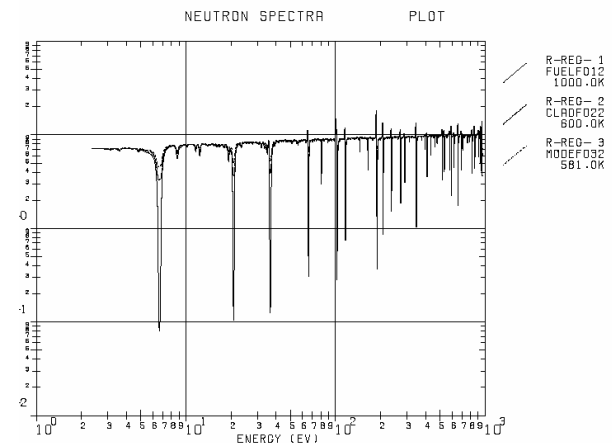
Location and type of particles are sampled along a flight path of each neutron

# SRAC: neutronics calculation code system for various types of thermal reactors

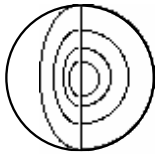
- Production of effective microscopic and macroscopic group cross sections
- Static cell and core calculations including burn-up analyses

## Features

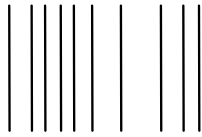
- Collision probability calculation (PIJ) applicable to 16 types of lattice geometries
- PEACO option which solves a multi-region cell problem by PIJ using hyper-fine lethargy mesh in resonance energy range
- SN transport codes ANISN(1D), TWOTRAN(2D) and multi-dimensional diffusion code CITATION are integrated into the system to enable many choices of calculation flow depending on problem



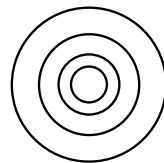
# Geometrical models of PIJ



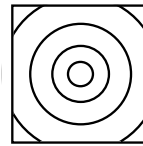
**Sphere**  
(Pebble, HTGR)



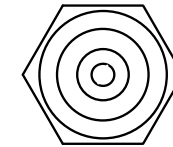
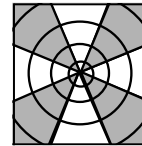
**1D-Plate**  
(JRR, JMTR)



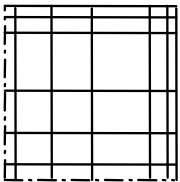
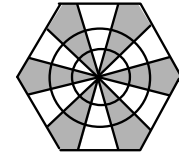
**1D-Cylinder**  
(any pin type fuel)



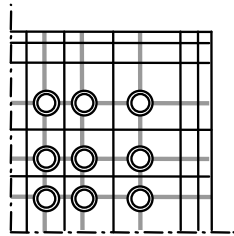
**Square unit pin cell**  
(PWR, BWR)



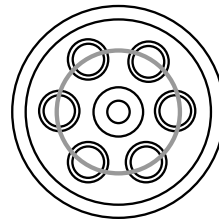
**Hexagonal unit pin cell**  
(FBR, VVER, HCLWR)



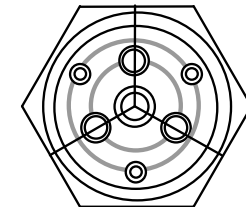
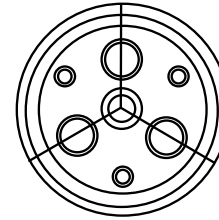
**2D square plate fuel assembly (KUCA)**



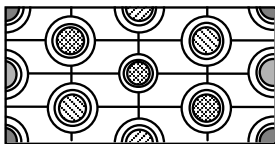
**2D square assembly with pin rods (PWR)**



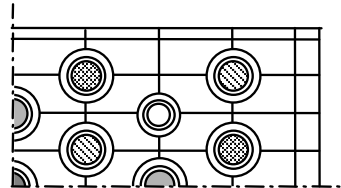
**Annular assembly with annular arrays of pin rods**  
(CANDU, ATR, RBMK)



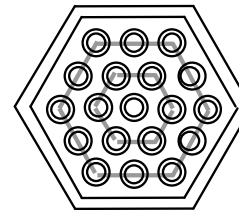
**Hexagonal assembly with annular arrays of pin rods (HTTR, VHTRC)**



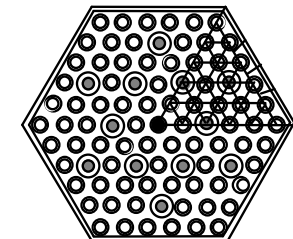
**Periodic 2D X-Y array with different pin rods (PROTEUS-LWHCR)**



**Reflective 2D X-Y array with different pin rods (PWR, BWR, etc.)**



**Hexagonal fuel assembly with pin rods (FBR)**

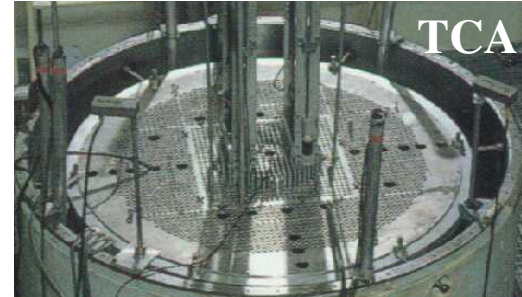


**Hexagonal Assembly with different types of pin rods (VVER, HCLWR)**

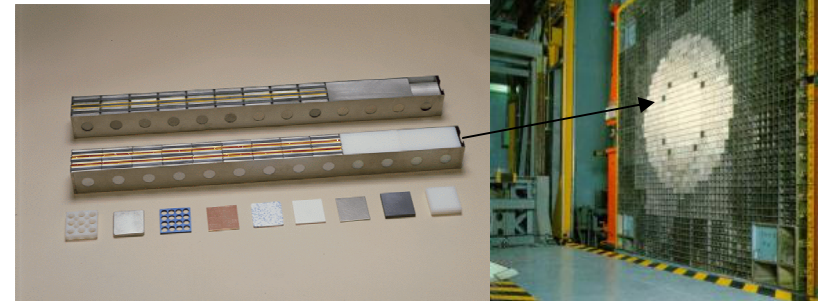
# Applications of MVP and SRAC in Japan

## Experimental Analyses of Critical Assemblies (CA) and Testing Reactors

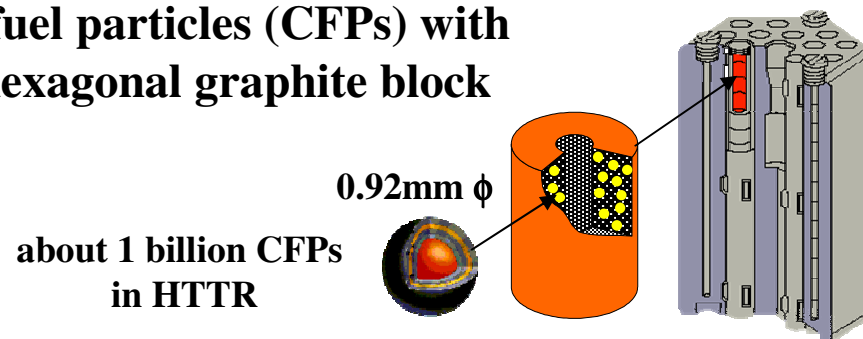
\***TCA** [JAERI]: Tank type critical assembly  
Pin type fuels (low enriched  $\text{UO}_2/\text{MOX}$ ),  
 $\text{H}_2\text{O}$  moderator



\***FCA** [JAERI]: Fast Critical Assembly  
Many kinds of plate type fuels and structural materials;  
uranium, plutonium, sodium, stainless steel, polyethylene, etc.



\***HTTR** [JAERI]: High Temperature engineering Test Reactor  
TRISO coated fuel particles (CFPs) with  
 $\text{UO}_2$  kernel in hexagonal graphite block  
fuel assembly



\***JMTRC** [JAERI] :CA for JAERI Material Testing Reactor

UAl<sub>x</sub>-Al plate type fuel,  
H<sub>2</sub>O moderator

\***STACY** [JAERI]: CA of Nucl. Fuel Cycle Safety

Engineering Research Facility (NUCEF)  
10% enriched uranyl nitrate solution fuel

\***KUCA** [Kyoto Univ.]

High enriched U-Al alloy plate type fuel,  
polyethylene moderator

\***EOLE** [Cadarash]: Programs by CEA(France) and NUPEC, JNES

MOX-LWR mockup experiments ; MISTRAL, BASALA and FUBILA



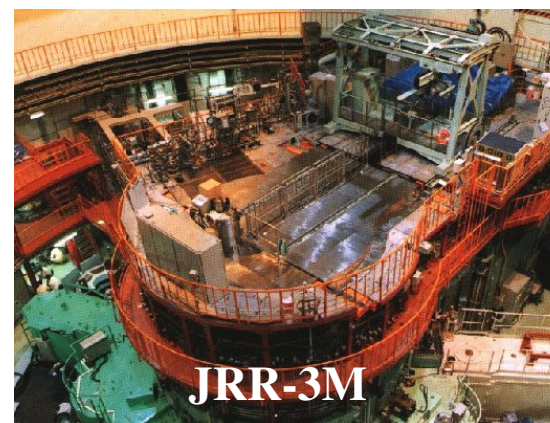
## Core Management and Upgrading of Research Reactor

\***JRR-2** [JAERI]: research reactor (decommissioned)

45% enriched UAl<sub>x</sub>-Al cylindrical plate type fuel,  
D<sub>2</sub>O moderator

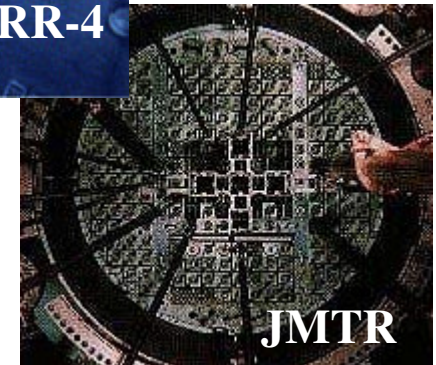
\***JRR-3M** [JAERI]: research reactor

20% enriched UAl<sub>x</sub>-Al plate type fuel,  
H<sub>2</sub>O moderator



**\*JRR-4 [JAERI]: research reactor**  
93% enriched U, U-Al alloy fuel, (~1996)  
20% enriched U,  $U_3Si_2$ -Al dispersed alloy  
fuel (~1998), H<sub>2</sub>O moderator

**\*JMTR [JAERI]: materials testing reactor**  
20% enriched  $U_3Si_2$ -Al dispersed alloy fuel,  
H<sub>2</sub>O moderator

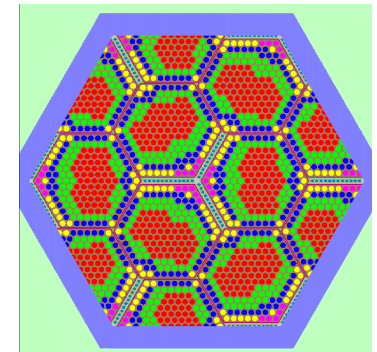


## Analyses of Post Irradiation Experiments

- \*PWR (Mihama NPP/Unit-3, Takahama NPP/Unit-3) by JAERI
- \*BWR (Fukushima NPP/Unit-1/3) by NUPEC
- \*REBUS program analyses by JNES

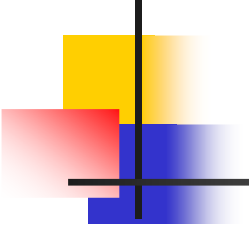
## Conceptual Nuclear Design Study of Future Reactors

- \*Reduced-Moderation Water Reactors
- \*Space Power Reactor
- \*Rock-like oxide (ROX) fueled Reactor



## Integral Test of JENDL

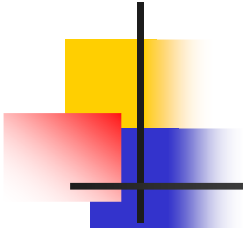
- \*Benchmark calculations for more than 1000 experiments is now in progress  
for next JENDL



## 6 . Future Plan and Conclusions

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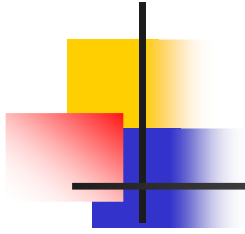
- LWR Assembly Calculation
  - Multi-group transport theory method with heterogeneous geometry
  - Anisotropic scattering
- LWR Core Calculation
  - 3-D multi-group cell averaged pin-by-pin transport calculation (SCOPE2)



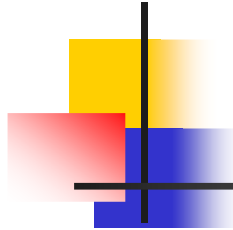
- Boundary between Assembly and Core calculations will disappear.

### Example

- CASMO-4 heterogeneous fuel-core transport calculation
- 2-D core calculation by PARAGON
- Micro Reactor Physics
  - Osaka University (Doppler Reactivity Effect)
  - PARAGON



- General
  - Monte-Carlo transient
  - Detailed Coupled system with Neutronic and Thermal-Hydraulic
- FR
  - Multi-group pin-by-pin fuel core transport



# Conclusion

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A lot of R&D Activities are being carried out for the improvement for LWR and FR Applications.